

**PPA MANUFACTURING PROCESS  
EMISSIONS TEST REPORT  
TEST DATES: 07-08 JANUARY 2019**

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FAYETTEVILLE, NORTH CAROLINA**

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# **1. INTRODUCTION**

## **1.1 FACILITY AND BACKGROUND INFORMATION**

The Chemours Fayetteville Works (Chemours) is located in Bladen County, North Carolina, approximately 10 miles south of the city of Fayetteville. The Chemours operating areas on the site include the Fluoromonomers, IXM and Polymer Processing Aid (PPA) manufacturing areas, Wastewater Treatment, and Powerhouse.

Chemours contracted Weston Solutions, Inc. (Weston) to perform HFPO Dimer Acid emission testing on the PPA Stack. Testing was performed on 7-8 January 2019 and generally followed the “Emissions Test Protocol” reviewed and approved by the North Carolina Department of Environmental Quality (NCDEQ). This report provides the results from the emission test program.

## **1.2 TEST OBJECTIVES**

The specific objectives for this test program were as follows:

- Measure the emissions concentrations and mass emissions rates of HFPO Dimer Acid from the PPA process stack which is located in the PPA process area.
- Monitor and record process data in conjunction with the test program.
- Provide representative emissions data.

## **1.3 TEST PROGRAM OVERVIEW**

During the emissions test program, the concentrations and mass emissions rates of HFPO Dimer Acid were measured on the PPA process stack source.

Table 1-1 provides a summary of the test locations and the parameters that were measured along with the sampling/analytical procedures that were followed.

Section 2 provides a summary of test results. A description of the processes is provided in Section 3. Section 4 provides a description of the test locations. The sampling and analytical procedures are provided in Section 5. Detailed test results and discussion are provided in Section 6.

Appendix C includes the summary reports for the laboratory analytical results. The full laboratory data packages are provided in electronic format and on CD with each hard copy.

**Table 1-1  
Sampling Plan for PPA Process Stack**

Sampling Point & Location	PPA Process Stack				
Number of Tests:	3				
Parameters To Be Tested:	HFPO Dimer Acid (HFPO-DA)	Volumetric Flow Rate and Gas Velocity	Carbon Dioxide	Oxygen	Water Content
Sampling or Monitoring Method	EPA M-0010	EPA M1, M2, M3A, and M4 in conjunction with M-0010 tests	EPA M3A		EPA M4 in conjunction with M-0010 tests
Sample Extraction/ Analysis Method(s):	LC/MS/MS	NA <sup>6</sup>	NA		NA
Sample Size	> 1m <sup>3</sup>	NA	NA	NA	NA
Total Number of Samples Collected <sup>1</sup>	3	3	3	3	3
Reagent Blanks (Solvents, Resins) <sup>1</sup>	1 set	0	0	0	0
Field Blank Trains <sup>1</sup>	1 per source	0	0	0	0
Proof Blanks <sup>1</sup>	1 per train	0	0	0	0
Trip Blanks <sup>1,2</sup>	1 set	0	0	0	
Lab Blanks	1 per fraction <sup>3</sup>	0	0	0	0
Laboratory or Batch Control Spike Samples (LCS)	1 per fraction <sup>3</sup>	0	0	0	0
Laboratory or Batch Control Spike Sample Duplicate (LCSD)	1 per fraction <sup>3</sup>	0	0	0	0
Media Blanks	1 set <sup>4</sup>	0	0	0	0
Isotope Dilution Internal Standard Spikes	Each sample	0	0	0	0
Total No. of Samples	7 <sup>5</sup>	3	3	3	3

Key:

<sup>1</sup> Sample collected in field.

<sup>2</sup> Trip blanks include one XAD-2 resin module and one methanol sample per sample shipment.

<sup>3</sup> Lab blank and LCS/LCSD includes one set per analytical fraction (front half, back half and condensate).

<sup>4</sup> One set of media blank archived at laboratory at media preparation.

<sup>5</sup> Actual number of samples collected in field.

<sup>6</sup> Not applicable.

## 2. SUMMARY OF TEST RESULTS

A total of three test runs were performed on the PPA process stack. Table 2-1 provides a summary of the HFPO Dimer Acid emission test results. Detailed test results summaries are provided in Section 6.

It is important to note that emphasis is being placed on the characterization of the emissions based on the stack test results. Research conducted in developing the protocol for stack testing HFPO Dimer Acid Fluoride, HFPO Dimer Acid Ammonium Salt and HFPO Dimer Acid realized that the resulting testing, including collection of the air samples and extraction of the various fraction of the sampling train, would result in all three compounds being expressed as simply the HFPO Dimer Acid. However, it should be understood that the total HFPO Dimer Acid results provided on Table 2-1 and in this report include a percentage of each of the three compounds.

**Table 2-1**

**Summary of HFPO Dimer Acid Test Results**

Source	Run No.	Emission Rates	
		lb/hr	g/sec
PPA Process Stack	1	1.32E-04	1.66E-05
	2	1.40E-04	1.76E-05
	3	1.14E-04	1.44E-05
	Average	1.29E-04	1.62E-05



### **3. PROCESS DESCRIPTIONS**

The PPA area is included in the scope of this test program.

#### **3.1 POLYMER PROCESSING AID (PPA) AREA**

The PPA facility produces surfactants used to produce fluoropolymer products at other Chemours facilities, such as Teflon®, as well as sales to outside producers of fluoropolymers.

Process streams are vented to a caustic wet scrubber (ACD-A1), carbon bed and vented to a process stack (AEP-A1). The process inside the building is under negative pressure and the building air is vented to the process stack (AEP-A1) and the carbon bed.

### 3.2 PROCESS OPERATIONS AND PARAMETERS

Source	Operation/Product	Batch or Continuous
PPA	AF Column Reboiler/Virgin	Continuous once it starts taking off to feed tank
	Pressure Transfers/Virgin or Purified	Batch (pressure transfers from one vessel to another – every 2 hours)

During the test program, the following parameters were monitored by Chemours and are included in Appendix A.

- PPA Process
  - Caustic Wet Scrubber (ACD-A1)
    - Caustic recirculation flow rate
    - Differential pressure across the packing

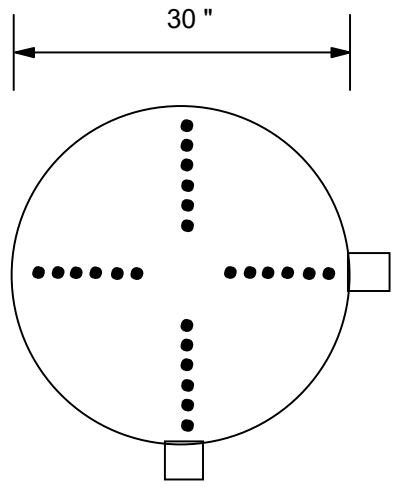
## **4. DESCRIPTION OF TEST LOCATIONS**

### **4.1 PPA PROCESS STACK**

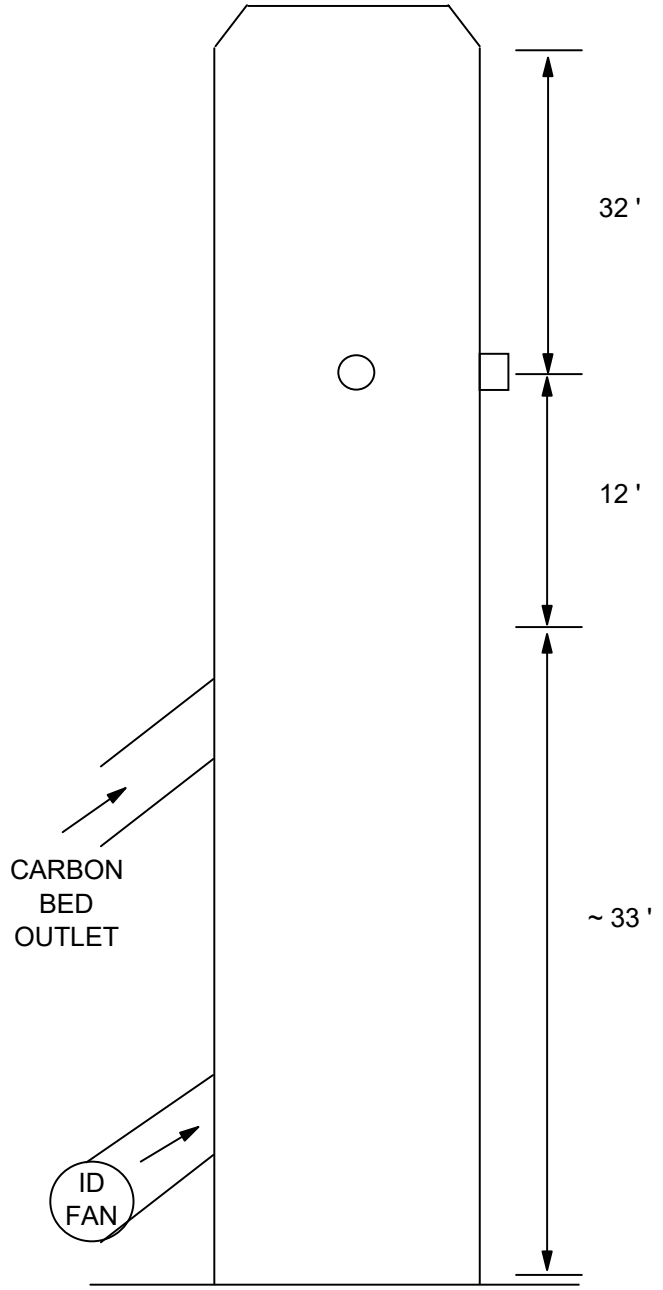
Two 4-inch ID test ports are in place on the 30-inch ID fiberglass stack. The ports are 12 feet (4.8 diameters) from the nearest downstream disturbance (carbon bed outlet) and 32 feet (12.8 diameters) from the nearest upstream disturbance (stack exit).

Per EPA Method 1, a total of 24 traverse points (12 per axis) were used for M-0010 isokinetic sampling. See Figure 4-1 for a schematic of the test port and traverse point locations.

Note: All measurements at the test location were confirmed prior to sampling.



TRAVERSE POINT NUMBER	DISTANCE FROM INSIDE NEAR WALL (INCHES)
1	1
2	2
3	3 1/2
4	5 3/8
5	7 1/2
6	10 3/4
7	19 3/8
8	22 1/2
9	24 3/4
10	26 1/2
11	28
12	29



DRAWING NOT TO SCALE

**FIGURE 4-1  
PPA PROCESS STACK TEST PORT  
AND TRAVERSE POINT LOCATION**

## **5. SAMPLING AND ANALYTICAL METHODS**

### **5.1 STACK GAS SAMPLING PROCEDURES**

The purpose of this section is to describe the stack gas emissions sampling train and to provide details of the stack sampling and analytical procedures utilized during the emissions test program.

#### **5.1.1 Pre-Test Determinations**

Preliminary test data was obtained at the test location. Stack geometry measurements were measured and recorded, and traverse point distances verified. A preliminary velocity traverse was performed utilizing a calibrated S-type pitot tube and an inclined manometer to determine velocity profiles. Flue gas temperatures were observed with a calibrated direct readout panel meter equipped with a chromel-alumel thermocouple. Preliminary water vapor content was estimated by wet bulb/dry bulb temperature measurements.

A check for the presence or absence of cyclonic flow was previously conducted at the test location. The cyclonic flow check was negative ( $< 20^\circ$ ) verifying that the source were acceptable for testing.

Preliminary test data was used for nozzle sizing and sampling rate determinations for isokinetic sampling procedures.

Calibration of probe nozzles, pitot tubes, metering systems, and temperature measurement devices was performed as specified in Section 5 of EPA Method 5 test procedures.

### **5.2 STACK PARAMETERS**

#### **5.2.1 EPA Method 0010**

The sampling train utilized to perform the HFPO Dimer Acid sampling was an EPA Method 0010 train (see Figure 5-1). The Method 0010 consisted of a borosilicate nozzle that attached directly to a heated borosilicate probe. In order to minimize possible thermal degradation of the HFPO Dimer Acid, the probe and particulate filter were heated above stack temperature to

minimize water vapor condensation before the filter. The probe was connected directly to a heated borosilicate filter holder containing a solvent extracted glass fiber filter.

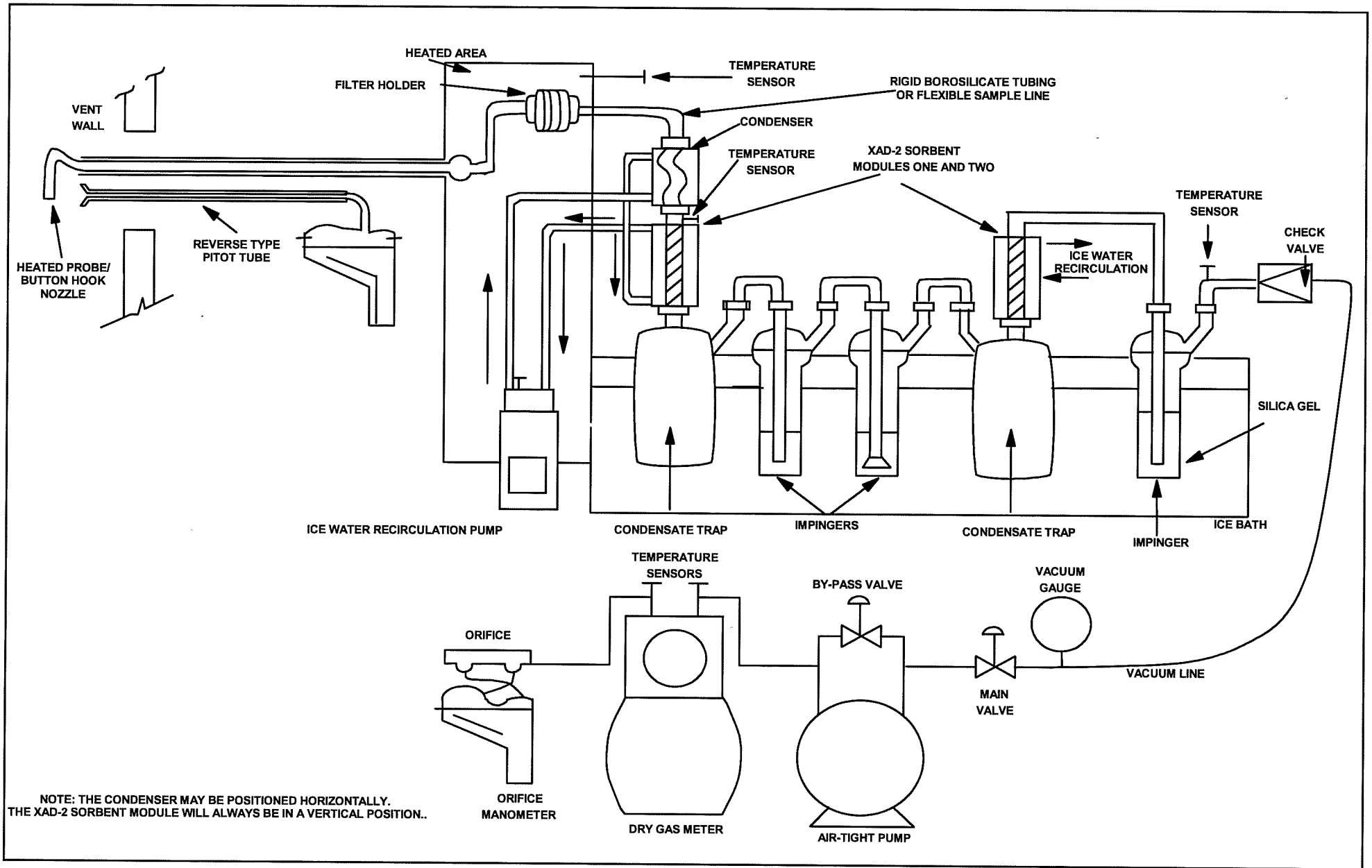


FIGURE 5-1  
EPA METHOD 0010 SAMPLING TRAIN

A section of borosilicate glass (or flexible polyethylene) tubing connected the filter holder exit to a Graham (spiral) type ice water-cooled condenser, an ice water-jacketed sorbent module containing approximately 40 grams of XAD-2 resin. The XAD-2 resin tube was equipped with an inlet temperature sensor. The XAD-2 resin trap was followed by a condensate knockout impinger and a series of two impingers that contained 100 milliliters of high purity distilled water. The train also included a second XAD-2 resin trap behind the impinger section to evaluate possible sampling train breakthrough. Each XAD-2 resin trap was connected to a 1-liter condensate knockout trap. The final impinger contained 300 grams of dry pre-weighed silica gel. All impingers and the condensate traps were maintained in an ice bath. Ice water was continuously circulated in the condenser and both XAD-2 modules to maintain method required temperature. A control console with a leakless vacuum pump, a calibrated orifice, and dual inclined manometers was connected to the final impinger via an umbilical cord to complete the sample train.

HFPO Dimer Acid Fluoride (CAS No. 2062-98-8) that is present in the stack gas is expected to be captured in the sampling train along with HFPO Dimer Acid (CAS No. 13252-13-6). HFPO Dimer Acid Fluoride undergoes hydrolysis instantaneously in water in the sampling train and during the sample recovery step and will be converted to HFPO Dimer Acid such that the amount of HFPO Dimer Acid emissions represents a combination of both HFPO Dimer Acid Fluoride and HFPO Dimer Acid.

During sampling, gas stream velocities were measured by attaching a calibrated S-type pitot tube into the gas stream adjacent to the sampling nozzle. The velocity pressure differential was observed immediately after positioning the nozzle at each traverse point, and the sampling rate adjusted to maintain isokineticity at  $100\% \pm 10$ . Flue gas temperature was monitored at each point with a calibrated panel meter and thermocouple. Isokinetic test data was recorded at each traverse point during all test periods, as appropriate. Leak checks were performed on the sampling apparatus according to reference method instructions, prior to and following each run, component change (if required), or during midpoint port changes.

### **5.2.2 EPA Method 0010 Sample Recovery**

At the conclusion of each test, the sampling train was dismantled, the openings sealed, and the components transported to the field laboratory trailer for recovery.



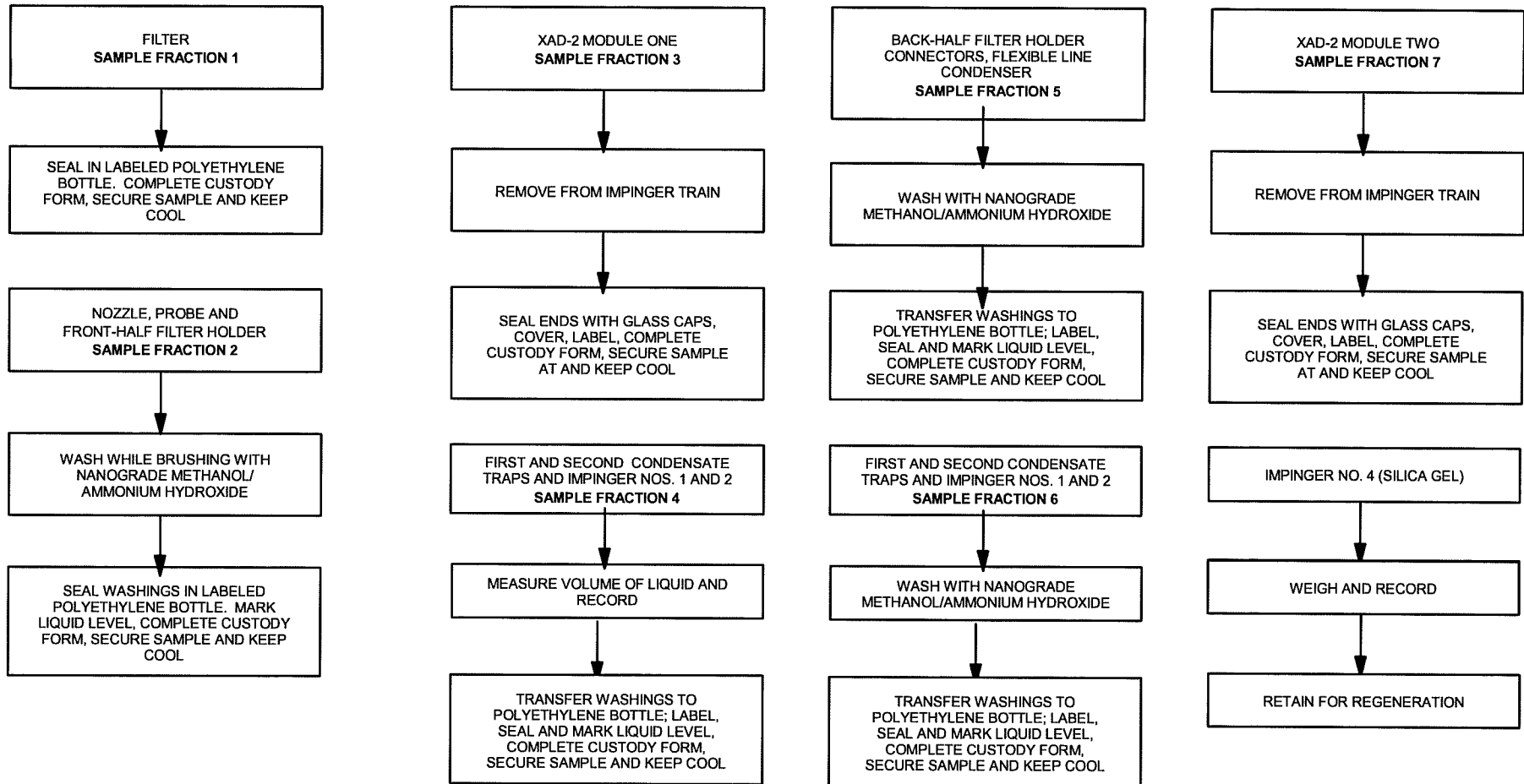
A consistent procedure was employed for sample recovery:

1. The two XAD-2 covered (to minimize light degradation) sorbent modules (1 and 2) were sealed and labeled.
2. The glass fiber filter(s) were removed from the holder with tweezers and placed in a polyethylene container along with any loose particulate and filter fragments.
3. The particulate adhering to the internal surfaces of the nozzle, probe and front half of the filter holder were rinsed with a solution of methanol and ammonium hydroxide into a polyethylene container while brushing a minimum of three times until no visible particulate remained. Particulate adhering to the brush was rinsed with methanol/ammonium hydroxide into the same container. The container was sealed.
4. The volume of liquid collected in the first condensate trap was measured, the value recorded, and the contents poured into a polyethylene container.
5. All train components between the filter exit and the first condensate trap were rinsed with methanol/ammonium hydroxide. The solvent rinse was placed in a separate polyethylene container and sealed.
6. The volume of liquid in impingers one and two, and the second condensate trap, were measured, the values recorded, and the sample was placed in the same container as Step 4 above, then sealed.
7. The two impingers, condensate trap, and connectors were rinsed with methanol/ammonium hydroxide. The solvent sample was placed in a separate polyethylene container and sealed.
8. The silica gel in the final impinger was weighed and the weight gain value recorded.
9. Site (reagent) blank samples of the methanol/ammonium hydroxide, XAD resin, filter and distilled water were retained for analysis.

Each container was labeled to clearly identify its contents. The height of the fluid level was marked on the container of each liquid sample to provide a reference point for a leakage check during transport. All samples were maintained cool.

During each test campaign, an M-0010 blank train was set up near the test location, leak checked and recovered along with the respective sample train. Following sample recovery, all samples were transported to TestAmerica Laboratories, Inc. (TestAmerica) for sample extraction and analysis.

See Figure 5-2 for a schematic of the M-0010 sample recovery process.



**FIGURE 5-2**  
**HFPO DIMER ACID SAMPLE RECOVERY PROCEDURES FOR METHOD 0010**

### 5.2.3 EPA Method 0010 – Sample Analysis

The Method 0010 sampling trains resulted in four separate analytical fractions for HFPO Dimer Acid analysis according to SW-846 Method 3542:

- Front-Half Composite—comprised of the particulate filter, and the probe, nozzle, and front-half of the filter holder solvent rinses;
- Back-Half Composite—comprised of the first XAD-2 resin material and the back-half of the filter holder with connecting glassware solvent rinses;
- Condensate Composite—comprised of the aqueous condensates and the contents of impingers one and two with solvent rinses;
- Breakthrough XAD-2 Resin Tube—comprised of the resin tube behind the series of impingers.

The second XAD-2 resin material was analyzed separately to evaluate any possible sampling train HFPO-DA breakthrough.

The front-half and back-half composites and the second XAD-2 resin material were placed in polypropylene wide-mouth bottles and tumbled with methanol containing 5% NH<sub>4</sub>OH for 18 hours. Portions of the extracts were processed analytically for the HFPO dimer acid by liquid chromatography and dual mass spectroscopy (HPLC/MS/MS). The condensate composite was concentrated onto a solid phase extraction (SPE) cartridge followed by desorption from the cartridge using methanol. Portions of those extracts were also processed analytically by HPLC/MS/MS.

Samples were spiked with isotope dilution internal standard (IDA) at the commencement of their preparation to provide accurate assessments of the analytical recoveries. Final data was corrected for IDA standard recoveries.

TestAmerica developed detailed procedures for the sample extraction and analysis for HFPO Dimer Acid. These procedures were incorporated into the test protocol.

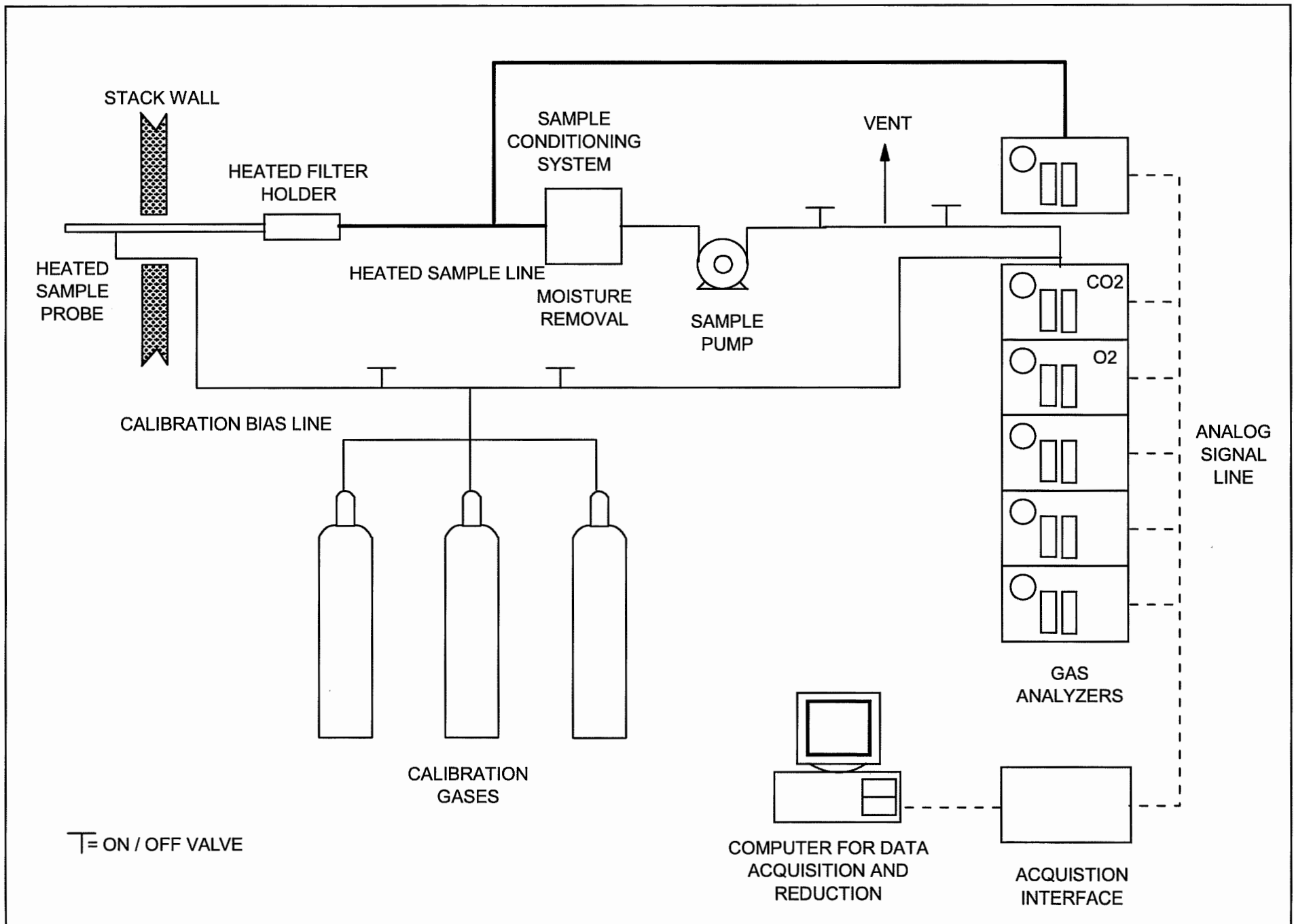
### 5.3 GAS COMPOSITION

The Weston mobile laboratory equipped with instrumental analyzers was used to measure carbon dioxide (CO<sub>2</sub>) and oxygen (O<sub>2</sub>) concentrations. A diagram of the Weston sampling system is presented in Figure 5-3.

Each analyzer was set up and calibrated internally by introduction of calibration gas standards directly to the analyzer from a calibration manifold. The calibration manifold is designed with an atmospheric vent to release excess calibration gas and maintains the calibration at ambient pressure. The direct calibration sequence consisted of alternate injections of zero and mid-range gases with appropriate adjustments until the desired responses were obtained. The high-range standards were then introduced in sequence without further adjustment.

The sample line integrity was verified by performing a bias test before and after each test period. The sampling system bias test consisted of introducing the zero gas and one up-range calibration standard in excess to the valve at the probe end when the system was sampling normally. The excess calibration gas flowed out through the probe to maintain ambient sampling system pressure. Calibration gas supply was regulated to maintain constant sampling rate and pressure. Instrument bias check response was compared to internal calibration responses to ensure sample line integrity and to calculate a bias correction factor after each run using the ratio of the measured concentration of the bias gas certified by the calibration gas supplier.

The oxygen and carbon dioxide content of each stack gas was measured according to EPA Method 3A procedures which incorporate the latest updates of EPA Method 7E. A Servomex Model 4900 analyzer (or equivalent) was used to measure oxygen content. A Servomex Model 4900 analyzer (or equivalent) was used to measure carbon dioxide content of the stack gas. Both analyzers were calibrated with EPA Protocol gases prior to the start of the test program and performance was verified by sample bias checks before and after each test run.



**FIGURE 5-3**  
**WESTON SAMPLING SYSTEM**

## 6. DETAILED TEST RESULTS AND DISCUSSION

Preliminary testing and the associated analytical results required significant sample dilution to bring the HFPO Dimer Acid concentration within instrument calibration, therefore, sample times and sample volumes were reduced for the formal test program. This was approved by the North Carolina Department of Environmental Quality (NCDEQ).

Each test was a minimum of 96 minutes in duration. A total of three test runs were performed on the PPA process stack.

Table 6-1 provides detailed test data and test results for the PPA process stack.

The Method 3A sampling on all sources indicated that the O<sub>2</sub> and CO<sub>2</sub> concentrations were at ambient air levels (20.9% O<sub>2</sub>, 0% CO<sub>2</sub>), therefore, 20.9% O<sub>2</sub> and 0% CO<sub>2</sub> values were used in all calculations.

**TABLE 6-1**  
**CHEMOURS - FAYETTEVILLE, NC**  
**SUMMARY OF HFPO DIMER ACID TEST DATA AND TEST RESULTS**  
**PPA PROCESS STACK**

**Test Data**

	1	2	3
Run number			
Location	PPA Stack	PPA Stack	PPA Stack
Date	01/07/19	01/08/19	01/08/19
Time period	1240-1430	0800-0950	1053-1255

**SAMPLING DATA:**

Sampling duration, min.	96.0	96.0	96.0
Nozzle diameter, in.	0.190	0.190	0.190
Cross sectional nozzle area, sq.ft.	0.000197	0.000197	0.000197
Barometric pressure, in. Hg	30.40	30.08	30.08
Avg. orifice press. diff., in H <sub>2</sub> O	0.71	0.59	0.62
Avg. dry gas meter temp., deg F	65.8	51.5	65.2
Avg. abs. dry gas meter temp., deg. R	526	511	525
Total liquid collected by train, ml	19.2	19.5	25.2
Std. vol. of H <sub>2</sub> O vapor coll., cu.ft.	0.9	0.9	1.2
Dry gas meter calibration factor	0.9915	0.9915	0.9915
Sample vol. at meter cond., dcf	44.005	40.425	42.900
Sample vol. at std. cond., dscf <sup>(1)</sup>	44.579	41.643	43.038
Percent of isokinetic sampling	103.6	103.7	106.6

**GAS STREAM COMPOSITION DATA:**

CO <sub>2</sub> , % by volume, dry basis	0.0	0.0	0.0
O <sub>2</sub> , % by volume, dry basis	20.9	20.9	20.9
N <sub>2</sub> , % by volume, dry basis	79.1	79.1	79.1
Molecular wt. of dry gas, lb/lb mole	28.84	28.84	28.84
H <sub>2</sub> O vapor in gas stream, prop. by vol.	0.020	0.022	0.027
Mole fraction of dry gas	0.980	0.978	0.973
Molecular wt. of wet gas, lb/lb mole	28.62	28.60	28.55

**GAS STREAM VELOCITY AND VOLUMETRIC FLOW DATA:**

Static pressure, in. H <sub>2</sub> O	0.23	0.23	0.23
Absolute pressure, in. Hg	30.42	30.10	30.10
Avg. temperature, deg. F	62	73	68
Avg. absolute temperature, deg.R	522	533	528
Pitot tube coefficient	0.84	0.84	0.84
Total number of traverse points	24	24	24
Avg. gas stream velocity, ft./sec.	37.7	36.3	36.4
Stack/duct cross sectional area, sq.ft.	4.90	4.90	4.90
Avg. gas stream volumetric flow, wacf/min.	11073	10677	10703
Avg. gas stream volumetric flow, dscf/min.	11155	10414	10470

<sup>(1)</sup> Standard conditions = 68 deg. F. (20 deg. C.) and 29.92 in Hg (760 mm Hg)

**TABLE 6-1 (cont.)**  
**CHEMOURS - FAYETTEVILLE, NC**  
**SUMMARY OF HFPO DIMER ACID TEST DATA AND TEST RESULTS**  
**PPA PROCESS STACK**

**TEST DATA**

	1	2	3
Run number			
Location	PPA Stack	PPA Stack	PPA Stack
Date	01/07/19	01/08/19	01/08/19
Time period	1240-1430	0800-0950	1053-1255

**LABORATORY REPORT DATA, ug.**

HFPO Dimer Acid	3.9945	4.2320	3.5520
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**EMISSION RESULTS, ug/dscm.**

HFPO Dimer Acid	3.16	3.59	2.91
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**EMISSION RESULTS, lb/dscf.**

HFPO Dimer Acid	1.98E-10	2.24E-10	1.82E-10
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**EMISSION RESULTS, lb/hr.**

HFPO Dimer Acid	1.32E-04	1.40E-04	1.14E-04
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**EMISSION RESULTS, g/sec.**

HFPO Dimer Acid	1.66E-05	1.76E-05	1.44E-05
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**APPENDIX A**  
**PROCESS OPERATIONS DATA**

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Date 1/7/2019

Time	1100	1100			1200			1300			1400			1500		
Stack Testing							Run 1 - 1240-1430									
A/F column Feed Ratev (pounds per hour)																
Charging water to Hyd - venting																
Charging Sulfuric acid - venting																
Hydrolysis - Wash Tank pressure Transfer to Hydrolysis																
Hydrolysis - Phase Settle									1:45 to 2:30							
Vap heels pressure transfer																
Vap cycle							12:45 to 1:30									
Venting after press tran from North/South Acid tank to Hyd																
DAF tran to Hyd - venting during transfer							12:45 to 1:45									
Hydrolysis - transfer to Waste Acid Trailer																
Scrubber Recirculation Flow	38 gpm															
Scrubber dP	less than 0.5 inwc															

Date 1/8/2019

Time	1100	800				900				1000				1100				1200									
Stack Testing		Run 2 - 0800-0950								Run 3 - 1053-1255																	
A/F column Feed Ratev (pounds per hour)																											
Charging water to Hyd - venting																											
Charging Sulfuric acid - venting																											
Hydrolysis - Wash Tank pressure Transfer to Hydrolysis																											
Hydrolysis - Phase Settle						8:45 to 9:30								No transfers													
Vap heels pressure transfer																											
Vap cycle																											
Venting after press tran from North/South Acid tank to Hyd																											
DAF tran to Hyd - venting during transfer			8 am to 8:45											No transfers													
Hydrolysis - transfer to Waste Acid Trailer																											
Scrubber Recirculation Flow		38 gpm for duration																									
Scrubber dP		less than 0.5 inwc for duration																									

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**APPENDIX B**  
**RAW AND REDUCED TEST DATA**

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**CHEMOURS - FAYETTEVILLE, NC**  
**INPUTS FOR HFPO DIMER ACID CALCULATIONS**  
**PPA PROCESS STACK**

**Test Data**

	1	2	3
Run number			
Location	PPA Stack	PPA Stack	PPA Stack
Date	01/07/19	01/08/19	01/08/19
Time period	1240-1430	0800-0950	1053-1255
Operator	AS/KS	JL/KS	JL/KS

**Inputs For Calcs.**

Sq. rt. delta P	0.67728	0.64296	0.64656
Delta H	0.7121	0.5946	0.6217
Stack temp. (deg.F)	62.0	72.6	68.1
Meter temp. (deg.F)	65.8	51.5	65.2
Sample volume (act.)	44.005	40.425	42.900
Barometric press. (in.Hg)	30.40	30.08	30.08
Volume H <sub>2</sub> O imp. (ml)	9.0	10.0	14.0
Weight change sil. gel (g)	10.2	9.5	11.2
% CO <sub>2</sub>	0.0	0.0	0.0
% O <sub>2</sub>	20.9	20.9	20.9
% N <sub>2</sub>	79.1	79.1	79.1
Area of stack (sq.ft.)	4.900	4.900	4.900
Sample time (min.)	96.0	96.0	96.0
Static pressure (in.H <sub>2</sub> O)	0.23	0.23	0.23
Nozzle dia. (in.)	0.190	0.190	0.190
Meter box cal.	0.9915	0.9915	0.9915
Cp of pitot tube	0.84	0.84	0.84
Traverse points	24	24	24

# Sample and Velocity Traverse Point Data Sheet - Method 1

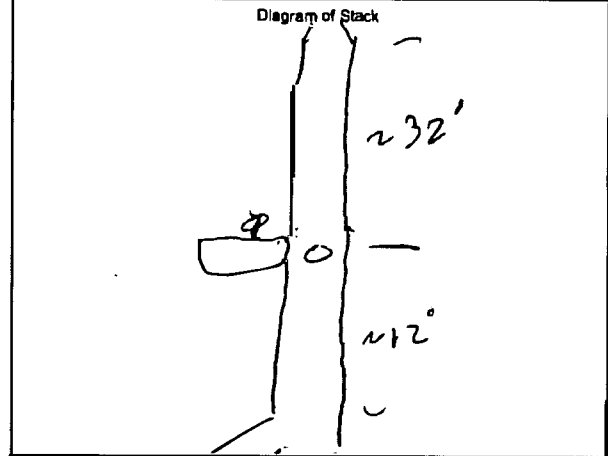
Client Chemours  
 Location/Plant Fayetteville NC  
 Source Ptd. stack

Operator Palm  
 Date 11/18/07  
 W.O. Number 13416-00007

Duct Type  Circular  Rectangular Duct Indicate appropriate type  
 Traverse Type  Particulate Traverse  Velocity Traverse  CEM Traverse

Distance from far wall to outside of port (in.) = C	45
Port Depth (in.) = D	15
Depth of Duct, diameter (in.) = C-D	30
Area of Duct (ft <sup>2</sup> )	4.90
Total Traverse Points	24
Total Traverse Points per Port	12
Port Diameter (in.) —(Flange-Threaded-Hole)	4"
Monorail Length	-
<b>Rectangular Ducts Only</b>	
Width of Duct, rectangular duct only (in.)	11.0
Total Ports (rectangular duct only)	1
Equivalent Diameter = (2*L*W)/(L+W)	

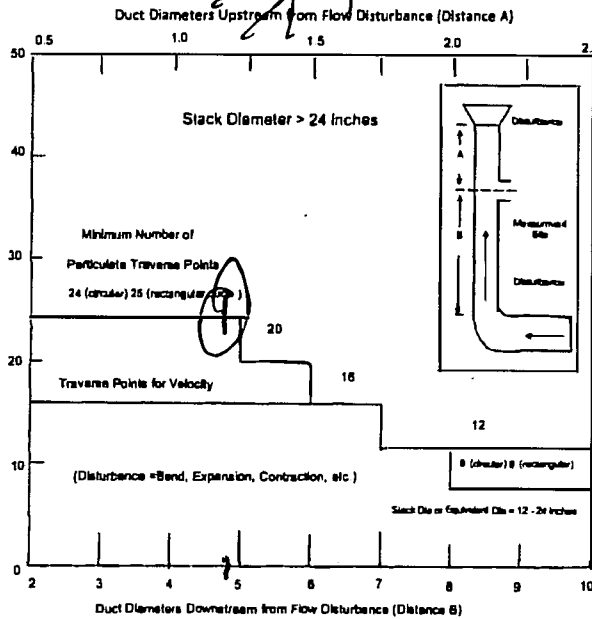
Flow Disturbances	
Upstream - A (ft)	132
Downstream - B (ft)	112
Upstream - A (duct diameters)	~12.8
Downstream - B (duct diameters)	~14.0



Traverse Point Locations			
Traverse Point	% of Duct	Distance from Inside Duct Wall (in)	Distance from Outside of Port (in)
1	2.1	6.3	16
2	6.7	20	17
3	11.0	30.5	18 1/2
4	17.7	51.3	20 3/8
5	25	75	22 1/2
6	35.0	105	25 3/4
7	44.4	133	34 3/8
8	55	165	37 1/2
9	67.3	201.7	39 3/4
10	80.2	240.6	46 1/2
11	93.3	280.0	47
12	97.5	292.5	47

CEM 3 Point (Long Measurement Line) Stratification Point Locations		
1	0.167	
2	0.50	
3	0.833	



Note: If stack dia < 12 inch use EPA Method 1A (Sample port upstream of pilot port)  
 Note: If stack dia > 24" then adjust traverse point to 1 inch from wall  
 If stack dia < 24" then adjust traverse point to 0.5 inch from wall

Traverse Point Location Percent of Stack -Circular													
		Number of Traverse Points											
		1	2	3	4	5	6	7	8	9	10	11	12
T	1		14.6		6.7		4.4		3.2		2.6		2.1
T	2		35.4		25		14.6		18.5		12		6.7
T	3			75		29.6		19.4		14.6		11.8	
T	4				93.3		70.4		52.3		22.6		17.7
T	5					85.4		67.7		34.2		25	
T	6						95.6		80.6		65.8		35.6
T	7							89.5		77.4		64.4	
T	8								96.8		85.4		75
T	9									91.8		82.3	
T	10										97.4		88.2
T	11											93.3	
T	12												97.5

Traverse Point Location Percent of Stack -Rectangular													
		Number of Traverse Points											
		1	2	3	4	5	6	7	8	9	10	11	12
T	1		25.0	16.7	12.5	10.0	8.3	7.1	6.3	5.6	5.0	4.5	4.2
T	2		75.0	50.0	37.5	30.0	25.0	21.4	18.8	16.7	15.0	13.6	12.5
T	3			83.3	62.5	50.0	41.7	35.7	31.3	27.8	25.0	22.7	20.8
T	4				87.5	70.0	58.3	50.0	43.8	38.9	35.0	31.8	29.2
T	5					90.0	75.0	64.3	56.3	50.0	45.0	40.9	37.5
T	6						91.7	78.6	68.8	61.1	55.0	50.0	45.8
T	7							92.9	81.3	72.2	65.0	59.1	54.2
T	8								93.8	83.3	75.0	68.2	62.4
T	9									94.4	85.0	77.3	70.8
T	10										95.0	86.4	79.2
T	11											95.5	87.5
T	12												95.8



# ISOKINETIC FIELD DATA SHEET

## Method 0010 HFPO Dimer Acid

Client: Chemours  
 W.O.#: 15418.002.009.0001  
 Project ID: Chemours  
 Mode/Source ID: PPA  
 Samp. Loc. ID: STK  
 Run No. ID: 1  
 Test Method ID: M 0010 HFPO Dimer Acid  
 Date ID: 7JAN2019  
 Source/Location: PPA Stack  
 Sample Date: 1-7-2019  
 Baro. Press (in Hg): 30.40  
 Operator: AS/KS

**Stack Conditions**

Assumed	Actual
2	9
	10.7
0	0.3
20.9	20.9
55	
65	
.23	0.23
	57.0

Meter Box ID: 21  
 Meter Box Y: .9915 ✓  
 Meter Box Del H: 2.0089  
 Probe ID / Length: 696 / 51  
 Probe Material: Boro  
 Pitot / Thermocouple ID: 696  
 Pitot Coefficient: 0.84  
 Nozzle ID: .190  
 Avg Nozzle Dia (in): .190 ✓  
 Area of Stack (ft²): 4.90 ✓  
 Sample Time: 96 min ✓  
 Total Traverse Pts: 24 ✓

K Factor: 1.55

Initial	Mid-Point	Final
.001	.000	.000
15"	51"	51"
yes / no	yes / no	yes / no
yes / no	yes / no	yes / no
Pre-Test Set		Post-Test Set
58		60
57.2		57.1
Pass / Fail		Pass / Fail
yes / no		yes / no

TRAVERSE POINT NO.	SAMPLE TIME (min)	CLOCK TIME (plant time)	VELOCITY PRESSURE Delta P (in H2O)	ORIFICE PRESSURE Delta H (in H2O)	DRY GAS METER READING (ft³)	STACK TEMP (°F)	DGM INLET TEMP (°F)	DGM OUTLET TEMP (°F)	PROBE TEMP (°F)	FILTER BOX TEMP (F)	IMPINGER EXIT TEMP (°F)	SAMPLE TRAIN VAC (in Hg)	XAD	COMMENTS
	0	1240			116.686									
A1	4		.55	.85	113.8	57	59.2	60	253	252	58	3	59	
2	8		.53	.82	115.8	62		63	125	123	60	3	61	
3	12		.54	.83	117.8	61		62	129	130	59	3	58	
4	16		.53	.82	119.8	60		61	120	123	59	3	58	
5	20		.53	.82	121.8	61		64	120	130	59	3	58	
6	24		.51	.79	123.8	61		63	119	125	59	3	60	
7	28		.45	.69	125.8	61		65	119	123	61	3	60	
8	32		.45	.69	127.5	61		65	119	124	58	3	58	
9	36		.40	.62	129.2	63		65	119	124	60	3	62	
10	40		.36	.55	131.0	62		64	121	125	57	2	58	
11	44		.36	.55	132.5	61		65	121	124	61	2	60	
12	48	1328	.30 ✓	.46 ↓	134.071 ✓	61 ✓		67 ✓	120	123	60	2	59	
									120.2	128.2	61.2		60.2	135.218
B1	52	1342	.53	.82	136.2	61		66	120	125	61	3	60	-1.147 LC
2	56		.53	.82	138.2	61		68	119	124	63	3	63	
3	60		.54	.83	140.2	61		67	119	124	60	3	60	
4	64		.53	.82	142.2	62		66	121	124	61	3	62	
5	68		.53	.82	144.3	66		68	121	124	66	3	60	
6	72		.49	.75	146.2	61		67	121	124	59	3	59	
7	76		.49	.75	148.2	61		67	121	124	59	3	60	
8	80		.48	.74	150.1	61		68	119	123	60	2.5	60	
9	84		.45	.69	151.9	66		70	121	123	64	2.5	64	
10	88		.36	.55	153.9	67		69	120	124	60	2	60	
11	92		.36	.55	155.3	63		69	120	124	60	2	60	
12	96	1430	.30 ✓	.46 ✓	156.838 ✓	64 ✓		69 ✓	120	124	61	2	62	

Avg Sqrt Delta P: 0.6773 ✓  
 Avg Delta H: 0.7121 ✓  
 Total Volume: 44.005 ✓  
 Avg Ts: 61.9 ✓  
 Avg Tm: 65.8 ✓  
 Min/Max: 119 / 123 ✓  
 Min/Max: 123 / 124 ✓  
 Max Temp: 66 ✓  
 Max Vac: 3 ✓  
 Max Temp: 63 ✓

Avg: 0.4625 ✓  
 Avg Sqrt Del H: 0.8403 ✓

Comments:



✓

# ISOKINETIC FIELD DATA SHEET

## Method 0010 HFPO Dimer Acid

Page \_\_\_ of \_\_\_

Client: Chemours  
 W.O.#: 15418.002.009.0001  
 Project ID: Chemours  
 Mode/Source ID: PPA  
 Samp. Loc. ID: STK  
 Run No. ID: 2  
 Test Method ID: M 0010 HFPO Dimer Acid  
 Date ID: 7JAN2019  
 Source/Location: PPA Stack  
 Sample Date: 01/08/19  
 Baro. Press (in Hg): 30.08 ✓  
 Operator: SL/KS ✓

**Stack Conditions**

Assumed	Actual
2	
	10
	9.5
0	0.0
20.9	20.9
65	
0.23 ✓	0.23 ✓
50°	

Meter Box ID: 21  
 Meter Box Y: 0.9915 ✓  
 Meter Box Del H: 2.0089 ✓  
 Probe ID / Length: 696 | 5'  
 Probe Material: Boro  
 Pitot / Thermocouple ID: 696 | 696  
 Pitot Coefficient: 0.84  
 Nozzle ID: 0.196  
 Avg Nozzle Dia (in): 0.190 ✓  
 Area of Stack (ft²): 4.90 ✓  
 Sample Time: 96 ✓  
 Total Traverse Pts: 24 ✓

K Factor: 1.87 1.44

Initial	Mid-Point	Final
0.001	0.001	0.006
5"	5"	5"
yes / no	yes / no	yes / no
yes / no	yes / no	yes / no
Pre-Test Set		Post-Test Set
53		54
52.5		53.5
Pass / Fail		Pass / Fail
yes / no		yes / no

TRAVERSE POINT NO.	SAMPLE TIME (min)	CLOCK TIME (plant time)	VELOCITY PRESSURE Delta P (in H2O)	ORIFICE PRESSURE Delta H (in H2O)	DRY GAS METER READING (ft³)	STACK TEMP (°F)	DGM INLET TEMP (°F)	DGM OUTLET TEMP (°F)	PROBE TEMP (°F)	FILTER BOX TEMP (F)	IMPINGER EXIT TEMP (°F)	SAMPLE TRAIN VAC (in Hg)	XAD	COMMENTS
	0	0800			157.495									
A1	4		.48	.69	159.2	74	54	54	119	124	57	2	53	
2	8		.48	.69	161.0	76	51	51	119	124	52	2	40	
3	12		.48	.69	163.0	76	50	50	119	124	49	2	38	
4	16		.48	.69	164.6	73	49	49	119	124	46	2	38	
5	20		.47	.67	166.4	73	49	49	121	123	45	2	39	
6	24		.46	.66	168.2	73	49	49	121	124	43	2	37	
7	28		.46	.66	169.9	73	49	49	121	124	43	2	36	
8	32		.42	.60	171.6	72	49	49	121	124	42	2	36	
9	36		.42	.60	173.3	72	49	49	119	124	41	2	36	
10	40		.40	.57	175.0	72	49	49	119	125	42	2	37	
11	44		.40	.57	176.6	71	50	50	120	124	42	2	36	178.554
12	48	0849	.40 ✓	.57 ✓	178.352	71 ✓	50 ✓	50 ✓	120	124	42	2	37	-1202 LC
B1	52	0902	.30	.43	180.0	70	50	50	119	124	47	2	41	
2	56		.32	.46	181.5	72	51	51	119	124	43	2	36	
3	60		.46	.66	183.2	72	51	51	120	124	43	2	35	
4	64		.46	.66	185.0	72	51	51	121	124	43	2	36	
5	69		.46	.66	186.8	72	52	52	121	124	42	2	35	
6	72		.44	.63	188.6	72	52	52	119	124	41	2	35	
7	76		.40	.57	190.3	72	53	53	121	124	42	2	36	
8	80		.40	.57	191.9	72	54	54	121	124	43	2	36	
9	84		.38	.54	193.5	73	55	55	121	124	43	2	37	
10	88		.36	.51	195.1	73	56	56	121	124	44	2	37	
11	92		.32	.46	196.6	73	56	56	120	124	45	2	38	
12	96	0950	.32 ✓	.46 ✓	198.122	73 ✓	56 ✓	56 ✓	120	124	46	2	38	
			Avg Sqrt Delta P	Avg Delta H	Total Volume	Avg Ts ✓	Avg Tm	Min/Max	Min/Max	Max Temp	Max Vac	Max Temp		
			415.645	154.458	40.425 ✓	72.583	51.458 ✓	119/121	124/125	57	2	53		
			415.4	176.99	Comments:									



W = 0.64206

✓



# ISOKINETIC FIELD DATA SHEET

# Method 0010 HFPO Dimer Acid

Client: Chemours  
 W.O.#: 15418.002.009.0001  
 Project ID: Chemours  
 Mode/Source ID: PPA  
 Samp. Loc. ID: STK  
 Run No. ID: 3  
 Test Method ID: M 0010 HFPO Dimer Acid  
 Date ID: 7JAN2019  
 Source/Location: PPA Stack  
 Sample Date: 01/08/19  
 Baro. Press (in Hg): 30.08  
 Operator: JL/KS

**Stack Conditions**

Assumed	Actual
2	210.14
0	29.5/1.2
20.9	20.9
75	65
0.23	0.23
61°	

Meter Box ID: 21  
 Meter Box Y: 9915  
 Meter Box Del H: 2.0059  
 Probe ID / Length: 696 / 5'  
 Probe Material: Boro  
 Pitot / Thermocouple ID: 696 / 696  
 Pitot Coefficient: 0.84  
 Nozzle ID: 190  
 Avg Nozzle Dia (in): 190  
 Area of Stack (ft²): 4.90  
 Sample Time: 46  
 Total Traverse Pts: 24

K Factor: 1.49

Initial	Mid-Point	Final
0.001	0.001	0.001
15"	5"	5"
yes / no	yes / no	yes / no
yes / no	yes / no	yes / no
Pre-Test Set		Post-Test Set
60		60
60.8		59.9
Pass / Fail		Pass / Fail
yes / no		yes / no

TRAVERSE POINT NO.	SAMPLE TIME (min)	CLOCK TIME (plant time)	VELOCITY PRESSURE Delta P (in H2O)	ORIFICE PRESSURE Delta H (in H2O)	DRY GAS METER READING (ft³)	STACK TEMP (°F)	DGM INLET TEMP (°F)	DGM OUTLET TEMP (°F)	PROBE TEMP (°F)	FILTER BOX TEMP (F)	IMPING EXIT TEMP (°F)	SAMPLE TRAIN VAC (in Hg)	XAD Exit	COMMENTS
	0	1059			200.710									
A1	4		.47	.70	202.9	61	60	60	119	124	61	2	61	
2	8		.47	.70	204.7	63	60	60	121	124	61	2	60	
3	12		.47	.70	206.6	63	60	60	121	124	61	2	60	
4	16		.47	.70	209.6	64	61	61	121	124	60	2	61	
5	20		.45	.67	210.2	64	61	61	121	123	61	2	62	
6	24		.46	.68	212.0	64	61	61	119	124	61	2	62	
7	28		.46	.68	213.9	64	61	61	119	124	61	2	62	
8	32		.34	.50	215.6	66	63	63	119	124	63	2	64	
9	36		.34	.50	217.1	69	64	64	122	125	64	2	66	
10	40		.34	.50	218.9	72	63	63	122	124	62	2	66	
11	44		.33	.49	219.9	72	64	64	120	124	57	2	55	
12	48	1141	.33	.49	221.858	72	65	65	120	124	57	2	54	222.297
											65		65	- .439 LC
B1	52	1204	.45	.67	224.6	67	67	67	119	126	65	2	65	
2	56		.45	.67	226.4	67	66	66	120	123	64	2	64	
3	60		.45	.67	228.1	68	67	67	120	124	64	2	65	
4	64		.46	.68	229.9	70	68	68	121	124	66	2	66	
5	68		.46	.68	231.8	71	68	68	119	124	60	2	55	
6	72		.46	.68	233.6	71	69	69	119	123	66	2	66	
7	76		.40	.59	235.4	68	68	68	120	124	66	2	66	
8	80		.40	.59	237.1	71	69	69	121	125	66	2	67	
9	84		.41	.61	238.8	70	69	69	119	123	66	2	67	
10	88		.40	.59	240.6	69	69	69	119	125	66	2	66	
11	92		.40	.59	242.3	72	71	71	119	125	67	2	66	
12	92	1255	.40	.59	244.049	72	71	71	119	124	66	2	67	

Avg Sqrt Delta P: 0.6465  
 Avg Delta H: 0.6211  
 Total Volume: 42.900  
 Avg Ts: 68.1  
 Avg Tm: 65.2  
 Min/Max: [blank]  
 Min/Max: [blank]  
 Max Temp: [blank]  
 Max Vac: [blank]  
 Max Temp: [blank]



# SAMPLE RECOVERY FIELD DATA

Method 0010 HFPO Dimer Acid

Client Chemours W.O. # 15418.002.009.0001  
 Location/Plant Fayetteville, NC Source & Location PPA Stack

Run No. 1 Sample Date 1/7/19 Recovery Date 1/7/19  
 Sample I.D. Chemours - PPA - STK - 1 - M 0010 HFPO Dimer Acid - Analyst PMM Filter Number NA

	Impinger							Imp.Total	8	Total
	1	2	3	4	5	6	7			
Contents									56	
Final	2	101	104	2					310.2	
Initial	0	100	100	0					300	
Gain	2	1	4	2				9	10.2	

Impinger Color clear Labeled?   
 Silica Gel Condition Good Sealed?

Run No. 2 Sample Date 1/8/19 Recovery Date 1/8/19  
 Sample I.D. Chemours - PPA - STK - 2 - M 0010 HFPO Dimer Acid - Analyst PMM Filter Number NA

	Impinger							Imp.Total	8	Total
	1	2	3	4	5	6	7			
Contents									56	
Final	2	89	108	1					309.5	
Initial	0	100	100	0					300	
Gain	2	-1	8	1				10	9.5	

Impinger Color clear Labeled?   
 Silica Gel Condition Good Sealed?

Run No. 3 Sample Date 1/8/19 Recovery Date 1/8/19  
 Sample I.D. Chemours - PPA - STK - 3 - M 0010 HFPO Dimer Acid - Analyst PMM Filter Number NA

	Impinger							Imp.Total	8	Total
	1	2	3	4	5	6	7			
Contents									56	
Final	14	102	96	4					311.2	
Initial	0	100	100	0					300	
Gain	14	0	-4	4				14	11.2	

Impinger Color clear Labeled?   
 Silica Gel Condition Good Sealed?

Check COC for Sample IDs of Media Blanks



# SAMPLE RECOVERY FIELD DATA

Method 0010 HFPO Dimer Acid

Client Chemours W.O. # 15418.002.009.0001  
 Location/Plant Fayetteville, NC Source & Location PPA Stack

Run No. \_\_\_\_\_ Sample Date 11/8/19 Recovery Date 1/2/20  
 Sample I.D. Chemours - PPA - STK - BT - M 0010 HFPO Dimer Aci Analyst VMM Filter Number VV

	Impinger								Imp.Total	8	Total
	1	2	3	4	5	6	7				
<b>Contents</b>											
<b>Final</b>	0	100	100	0						100	
<b>Initial</b>	0	100	100	0						100	
<b>Gain</b>	0	0	0	0						0	

Impinger Color clear Labeled? ✓  
 Silica Gel Condition good Sealed? ✓

Run No. \_\_\_\_\_ Sample Date \_\_\_\_\_ Recovery Date \_\_\_\_\_  
 Sample I.D. \_\_\_\_\_ Analyst \_\_\_\_\_ Filter Number \_\_\_\_\_

	Impinger								Imp.Total	8	Total
	1	2	3	4	5	6	7				
<b>Contents</b>											
<b>Final</b>											
<b>Initial</b>											
<b>Gain</b>											

Impinger Color \_\_\_\_\_ Labeled? \_\_\_\_\_  
 Silica Gel Condition \_\_\_\_\_ Sealed? \_\_\_\_\_

Run No. \_\_\_\_\_ Sample Date \_\_\_\_\_ Recovery Date \_\_\_\_\_  
 Sample I.D. \_\_\_\_\_ Analyst \_\_\_\_\_ Filter Number \_\_\_\_\_

	Impinger								Imp.Total	8	Total
	1	2	3	4	5	6	7				
<b>Contents</b>											
<b>Final</b>											
<b>Initial</b>											
<b>Gain</b>											

Impinger Color \_\_\_\_\_ Labeled? \_\_\_\_\_  
 Silica Gel Condition \_\_\_\_\_ Sealed? \_\_\_\_\_

Check COC for Sample IDs of Media Blanks



# METHODS AND ANALYZERS

Client: **Chemours**  
Location: **CHEMOURS**  
Source: **PPA**

Project Number: **15418.002.009**  
Operator: **CMH**  
Date: **7 Jan 2019**

---

**File:** C:\DATA\Chemours\010719 PPA stack.cem  
**Program Version:** 2.1, built 19 May 2017   **File Version:** 2.02  
**Computer:** WSWCAIRSERVICES   **Trailer:** 27  
**Analog Input Device:** Keithley KUSB-3108

---

## Channel 1

Analyte	<b>O<sub>2</sub></b>
Method	<b>EPA 3A, Using Bias</b>
Analyzer Make, Model & Serial No.	<b>Servomex 4900</b>
Full-Scale Output, mv	<b>10000</b>
Analyzer Range, %	<b>25.0</b>
Span Concentration, %	<b>21.0</b>

## Channel 2

Analyte	<b>CO<sub>2</sub></b>
Method	<b>EPA 3A, Using Bias</b>
Analyzer Make, Model & Serial No.	<b>Servomex 4900</b>
Full-Scale Output, mv	<b>10000</b>
Analyzer Range, %	<b>20.0</b>
Span Concentration, %	<b>16.6</b>

# CALIBRATION DATA

Number 1

Client: **Chemours**  
Location: **CHEMOURS**  
Source: **PPA**

Project Number: **15418.002.009**  
Operator: **CMH**  
Date: **7 Jan 2019**

---

Start Time: 11:24

**O<sub>2</sub>**

Method: EPA 3A

Calibration Type: Linear Zero and High Span

---

Calibration Standards

<b>%</b>	<b>Cylinder ID</b>
12.0	CC18055
21.0	SG9169108

---

Calibration Results

<b>Zero</b>	5 mv
<b>Span, 21.0 %</b>	7992 mv

---

Curve Coefficients

<b>Slope</b>	<b>Intercept</b>
380.3	5

---

**CO<sub>2</sub>**

Method: EPA 3A

Calibration Type: Linear Zero and High Span

---

Calibration Standards

<b>%</b>	<b>Cylinder ID</b>
8.9	CC18055
16.6	SG9169108

---

Calibration Results

<b>Zero</b>	5 mv
<b>Span, 16.6 %</b>	5516 mv

---

Curve Coefficients

<b>Slope</b>	<b>Intercept</b>
332.4	5

# CALIBRATION ERROR DATA

Number 1

Client: **Chemours**  
Location: **CHEMOURS**  
Source: **PPA**

Project Number: **15418.002.009**  
Operator: **CMH**  
Date: **7 Jan 2019**

Calibration 1

Start Time: 11:24

**O<sub>2</sub>**

Method: EPA 3A  
Span Conc. 21.0 %

Slope 380.3                      Intercept 5.0

Standard	Result	Difference	Error	Status
%	%	%	%	
Zero	0.0	0.0	0.0	Pass
12.0	12.0	0.0	0.0	Pass
21.0	21.0	0.0	0.0	Pass

**CO<sub>2</sub>**

Method: EPA 3A  
Span Conc. 16.6 %

Slope 332.4                      Intercept 5.0

Standard	Result	Difference	Error	Status
%	%	%	%	
Zero	0.0	0.0	0.0	Pass
8.9	8.7	-0.2	-1.2	Pass
16.6	16.6	0.0	0.0	Pass

# BIAS

Number 1

Client: **Chemours**  
Location: **CHEMOURS**  
Source: **PPA**

Project Number: **15418.002.009**  
Operator: **CMH**  
Date: **7 Jan 2019**

Calibration 1

Start Time: 11:39

**O<sub>2</sub>**

Method: EPA 3A  
Span Conc. 21.0 %

---

<b>Bias Results</b>					
<b>Standard</b>	<b>Cal.</b>	<b>Bias</b>	<b>Difference</b>	<b>Error</b>	<b>Status</b>
<b>Gas</b>	<b>%</b>	<b>%</b>	<b>%</b>	<b>%</b>	
<b>Zero</b>	0.0	0.0	0.0	0.0	Pass
<b>Span</b>	12.0	11.9	-0.1	-0.5	Pass

---

**CO<sub>2</sub>**

Method: EPA 3A  
Span Conc. 16.6 %

---

<b>Bias Results</b>					
<b>Standard</b>	<b>Cal.</b>	<b>Bias</b>	<b>Difference</b>	<b>Error</b>	<b>Status</b>
<b>Gas</b>	<b>%</b>	<b>%</b>	<b>%</b>	<b>%</b>	
<b>Zero</b>	0.0	0.0	0.0	0.0	Pass
<b>Span</b>	8.7	8.4	-0.3	-1.8	Pass

---

# RUN DATA

Number 1

Client: **Chemours**  
Location: **CHEMOURS**  
Source: **PPA**

Project Number: **15418.002.009**  
Operator: **CMH**  
Date: **7 Jan 2019**

Calibration 1

---

Time	O <sub>2</sub> %	CO <sub>2</sub> %
<b>Start R1</b>		
12:40	20.7	0.0
12:41	20.8	0.0
12:42	20.8	0.0
12:43	20.8	0.0
12:44	20.8	0.0
12:45	20.8	0.0
12:46	20.8	0.0
12:47	20.8	0.0
12:48	20.8	0.0
12:49	20.8	0.0
12:50	20.8	0.0
12:51	20.8	0.0
12:52	20.8	0.0
12:53	20.8	0.0
12:54	20.8	0.0
12:55	20.8	0.0
12:56	20.8	0.0
12:57	20.8	0.0
12:58	20.8	0.0
12:59	20.8	0.0
13:00	20.8	0.0
13:01	20.8	0.0
13:02	20.8	0.0
13:03	20.8	0.0
13:04	20.8	0.0
13:05	20.8	0.0
13:06	20.8	0.0
13:07	20.8	0.0
13:08	20.8	0.0
13:09	20.8	0.0
13:10	20.8	0.0
13:11	20.8	0.0
13:12	20.8	0.0
13:13	20.8	0.0
13:14	20.8	0.0
13:15	20.8	0.0
13:16	20.8	0.0
13:17	20.8	0.0
13:18	20.8	0.0
13:19	20.8	0.0

---



# RUN DATA

Number 1

Client: **Chemours**  
Location: **CHEMOURS**  
Source: **PPA**

Project Number: **15418.002.009**  
Operator: **CMH**  
Date: **7 Jan 2019**

Calibration 1

Time	O <sub>2</sub> %	CO <sub>2</sub> %
13:20	20.8	0.0
13:21	20.8	0.0
13:22	20.8	0.0
13:23	20.8	0.0
13:24	20.8	0.0
13:25	20.8	0.0
13:26	20.8	0.0
13:27	20.8	0.0
13:28	20.8	0.0
	<b>end port 1</b>	
	<b>port 2</b>	
13:42	20.7	0.0
13:43	20.8	0.0
13:44	20.8	0.0
13:45	20.8	0.0
13:46	20.8	0.0
13:47	20.8	0.0
13:48	20.8	0.0
13:49	20.8	0.0
13:50	20.8	0.0
13:51	20.8	0.0
13:52	20.8	0.0
13:53	20.8	0.0
13:54	20.8	0.0
13:55	20.8	0.0
13:56	20.8	0.0
13:57	20.8	0.0
13:58	20.8	0.0
13:59	20.8	0.0
14:00	20.8	0.0
14:01	20.8	0.0
14:02	20.8	0.0
14:03	20.8	0.0
14:04	20.8	0.0
14:05	20.8	0.0
14:06	20.8	0.0
14:07	20.8	0.0
14:08	20.8	0.0
14:09	20.8	0.0
14:10	20.8	0.0
14:11	20.8	0.0

# RUN DATA

Number 1

Client: **Chemours**  
Location: **CHEMOURS**  
Source: **PPA**

Project Number: **15418.002.009**  
Operator: **CMH**  
Date: **7 Jan 2019**

Calibration 1

---

Time	O <sub>2</sub> %	CO <sub>2</sub> %
14:12	20.8	0.0
14:13	20.8	0.0
14:14	20.8	0.0
14:15	20.8	0.0
14:16	20.8	0.0
14:17	20.8	0.0
14:18	20.8	0.0
14:19	20.8	0.0
14:20	20.8	0.0
14:21	20.8	0.0
14:22	20.8	0.0
14:23	20.8	0.0
14:24	20.8	0.0
14:25	20.8	0.0
14:26	20.8	0.0
14:27	20.8	0.0
14:28	20.8	0.0
14:30	20.8	0.0
<b>Avg</b>	<b>20.8</b>	<b>0.0</b>

---

# RUN SUMMARY

Number 1

Client: **Chemours**  
Location: **CHEMOURS**  
Source: **PPA**

Project Number: **15418.002.009**  
Operator: **CMH**  
Date: **7 Jan 2019**

Calibration 1

---

Method	O <sub>2</sub>	CO <sub>2</sub>
Conc. Units	EPA 3A	EPA 3A
	%	%

---

Time: 12:39 to 14:30

### Run Averages

20.8      0.0

### Pre-run Bias at 11:39

Zero Bias	0.0	0.0
Span Bias	11.9	8.4
Span Gas	12.0	8.9

### Post-run Bias at 14:34

Zero Bias	0.0	0.0
Span Bias	11.9	8.4
Span Gas	12.0	8.9

Run averages corrected for the average of the pre-run and post-run bias

21.0      0.0

# BIAS AND CALIBRATION DRIFT

Number 2

Client: **Chemours**  
Location: **CHEMOURS**  
Source: **PPA**

Project Number: **15418.002.009**  
Operator: **CMH**  
Date: **7 Jan 2019**

Calibration 1

Start Time: 14:34

**O<sub>2</sub>**

Method: EPA 3A  
Span Conc. 21.0 %

---

<b>Bias Results</b>					
<b>Standard</b>	<b>Cal.</b>	<b>Bias</b>	<b>Difference</b>	<b>Error</b>	<b>Status</b>
<b>Gas</b>	<b>%</b>	<b>%</b>	<b>%</b>	<b>%</b>	
<b>Zero</b>	0.0	0.0	0.0	0.0	Pass
<b>Span</b>	12.0	11.9	-0.1	-0.5	Pass

---

<b>Calibration Drift</b>					
<b>Standard</b>	<b>Initial*</b>	<b>Final</b>	<b>Difference</b>	<b>Drift</b>	<b>Status</b>
<b>Gas</b>	<b>%</b>	<b>%</b>	<b>%</b>	<b>%</b>	
<b>Zero</b>	0.0	0.0	0.0	0.0	Pass
<b>Span</b>	11.9	11.9	0.0	0.0	Pass

\*Bias No. 1

---

**CO<sub>2</sub>**

Method: EPA 3A  
Span Conc. 16.6 %

---

<b>Bias Results</b>					
<b>Standard</b>	<b>Cal.</b>	<b>Bias</b>	<b>Difference</b>	<b>Error</b>	<b>Status</b>
<b>Gas</b>	<b>%</b>	<b>%</b>	<b>%</b>	<b>%</b>	
<b>Zero</b>	0.0	0.0	0.0	0.0	Pass
<b>Span</b>	8.7	8.4	-0.3	-1.8	Pass

---

<b>Calibration Drift</b>					
<b>Standard</b>	<b>Initial*</b>	<b>Final</b>	<b>Difference</b>	<b>Drift</b>	<b>Status</b>
<b>Gas</b>	<b>%</b>	<b>%</b>	<b>%</b>	<b>%</b>	
<b>Zero</b>	0.0	0.0	0.0	0.0	Pass
<b>Span</b>	8.4	8.4	0.0	0.0	Pass

\*Bias No. 1

---

# METHODS AND ANALYZERS

Client: **Chemours**  
Location: **CHEMOURS**  
Source: **PPA**

Project Number: **15418.002.009**  
Operator: **CMH**  
Date: **8 Jan 2019**

---

**File:** C:\DATA\Chemours\010819 PPA.cem  
**Program Version:** 2.1, built 19 May 2017 **File Version:** 2.02  
**Computer:** WSWCAIRSERVICES **Trailer:** 27  
**Analog Input Device:** Keithley KUSB-3108

---

## Channel 1

Analyte	<b>O<sub>2</sub></b>
Method	<b>EPA 3A, Using Bias</b>
Analyzer Make, Model & Serial No.	<b>Servomex 4900</b>
Full-Scale Output, mv	<b>10000</b>
Analyzer Range, %	<b>25.0</b>
Span Concentration, %	<b>21.0</b>

## Channel 2

Analyte	<b>CO<sub>2</sub></b>
Method	<b>EPA 3A, Using Bias</b>
Analyzer Make, Model & Serial No.	<b>Servomex 4900</b>
Full-Scale Output, mv	<b>10000</b>
Analyzer Range, %	<b>20.0</b>
Span Concentration, %	<b>16.6</b>

# CALIBRATION DATA

Number 1

Client: **Chemours**  
Location: **CHEMOURS**  
Source: **PPA**

Project Number: **15418.002.009**  
Operator: **CMH**  
Date: **8 Jan 2019**

---

Start Time: 07:19

**O<sub>2</sub>**

Method: EPA 3A

Calibration Type: Linear Zero and High Span

---

Calibration Standards

%	Cylinder ID
12.0	CC18055
21.0	SG9169108

---

Calibration Results

<b>Zero</b>	30 mv
<b>Span, 21.0 %</b>	8006 mv

---

Curve Coefficients

Slope	Intercept
379.8	30

---

**CO<sub>2</sub>**

Method: EPA 3A

Calibration Type: Linear Zero and High Span

---

Calibration Standards

%	Cylinder ID
8.9	CC18055
16.6	SG9169108

---

Calibration Results

<b>Zero</b>	1 mv
<b>Span, 16.6 %</b>	5513 mv

---

Curve Coefficients

Slope	Intercept
332.4	1

# CALIBRATION ERROR DATA

Number 1

Client: **Chemours**  
Location: **CHEMOURS**  
Source: **PPA**

Project Number: **15418.002.009**  
Operator: **CMH**  
Date: **8 Jan 2019**

Calibration 1

Start Time: 07:19

**O<sub>2</sub>**

Method: EPA 3A

Span Conc. 21.0 %

Slope 379.8

Intercept 30.0

Standard	Result	Difference	Error	Status
%	%	%	%	
Zero	0.0	0.0	0.0	Pass
12.0	12.0	0.0	0.0	Pass
21.0	21.0	0.0	0.0	Pass

**CO<sub>2</sub>**

Method: EPA 3A

Span Conc. 16.6 %

Slope 332.4

Intercept 1.0

Standard	Result	Difference	Error	Status
%	%	%	%	
Zero	0.0	0.0	0.0	Pass
8.9	8.6	-0.3	-1.8	Pass
16.6	16.6	0.0	0.0	Pass

# BIAS

Number 1

Client: **Chemours**  
Location: **CHEMOURS**  
Source: **PPA**

Project Number: **15418.002.009**  
Operator: **CMH**  
Date: **8 Jan 2019**

Calibration 1

Start Time: 07:25

**O<sub>2</sub>**

Method: EPA 3A  
Span Conc. 21.0 %

---

<b>Bias Results</b>					
<b>Standard</b>	<b>Cal.</b>	<b>Bias</b>	<b>Difference</b>	<b>Error</b>	<b>Status</b>
<b>Gas</b>	<b>%</b>	<b>%</b>	<b>%</b>	<b>%</b>	
<b>Zero</b>	0.0	0.0	0.0	0.0	Pass
<b>Span</b>	12.0	12.0	0.0	0.0	Pass

---

**CO<sub>2</sub>**

Method: EPA 3A  
Span Conc. 16.6 %

---

<b>Bias Results</b>					
<b>Standard</b>	<b>Cal.</b>	<b>Bias</b>	<b>Difference</b>	<b>Error</b>	<b>Status</b>
<b>Gas</b>	<b>%</b>	<b>%</b>	<b>%</b>	<b>%</b>	
<b>Zero</b>	0.0	0.0	0.0	0.0	Pass
<b>Span</b>	8.6	8.4	-0.2	-1.2	Pass

---



# RUN DATA

Number 2

Client: **Chemours**  
Location: **CHEMOURS**  
Source: **PPA**

Project Number: **15418.002.009**  
Operator: **CMH**  
Date: **8 Jan 2019**

Calibration 1

---

Time	O <sub>2</sub> %	CO <sub>2</sub> %
<b>Start R2</b>		
08:00	20.8	0.0
08:01	20.8	0.0
08:02	20.8	0.0
08:03	20.8	0.0
08:04	20.8	0.0
08:05	20.8	0.0
08:06	20.8	0.0
08:07	20.8	0.0
08:08	20.8	0.0
08:09	20.8	0.0
08:10	20.8	0.0
08:11	20.8	0.0
08:12	20.8	0.0
08:13	20.8	0.0
08:14	20.8	0.0
08:15	20.8	0.0
08:16	20.8	0.0
08:17	20.8	0.0
08:18	20.8	0.0
08:19	20.8	0.0
08:20	20.8	0.0
08:21	20.8	0.0
08:22	20.8	0.0
08:23	20.9	0.0
08:24	20.9	0.0
08:25	20.9	0.0
08:26	20.9	0.0
08:27	20.9	0.0
08:28	20.9	0.0
08:29	20.9	0.0
08:30	20.9	0.0
08:31	20.9	0.0
08:32	20.9	0.0
08:33	20.9	0.0
08:34	20.9	0.0
08:35	20.9	0.0
08:36	20.9	0.0
08:37	20.9	0.0
08:38	20.9	0.0
08:39	20.9	0.0

---

# RUN DATA

Number 2

Client: **Chemours**  
Location: **CHEMOURS**  
Source: **PPA**

Project Number: **15418.002.009**  
Operator: **CMH**  
Date: **8 Jan 2019**

Calibration 1

---

Time	O <sub>2</sub> %	CO <sub>2</sub> %
08:40	20.9	0.0
08:41	20.9	0.0
08:42	20.9	0.0
08:43	20.9	0.0
08:44	20.9	0.0
08:45	20.9	0.0
08:46	20.9	0.0
08:47	20.9	0.0
08:48	20.9	0.0
	<b>end port 1</b>	
	<b>start port 2</b>	
09:02	20.8	0.0
09:03	20.8	0.0
09:04	20.9	0.0
09:05	20.9	0.0
09:06	20.9	0.0
09:07	20.9	0.0
09:08	20.9	0.0
09:09	20.9	0.0
09:10	20.9	0.0
09:11	20.9	0.0
09:12	20.9	0.0
09:13	20.9	0.0
09:14	20.9	0.0
09:15	20.9	0.0
09:16	20.9	0.0
09:17	20.9	0.0
09:18	20.9	0.0
09:19	20.9	0.0
09:20	20.9	0.0
09:21	20.9	0.0
09:22	20.9	0.0
09:23	20.9	0.0
09:24	20.9	0.0
09:25	20.9	0.0
09:26	20.9	0.0
09:27	20.9	0.0
09:28	20.9	0.0
09:29	20.9	0.0
09:30	20.9	0.0
09:31	20.9	0.0

---

# RUN DATA

Number 2

Client: **Chemours**  
Location: **CHEMOURS**  
Source: **PPA**

Project Number: **15418.002.009**  
Operator: **CMH**  
Date: **8 Jan 2019**

Calibration 1

---

Time	O <sub>2</sub> %	CO <sub>2</sub> %
09:32	20.9	0.0
09:33	20.9	0.0
09:34	20.9	0.0
09:35	20.9	0.0
09:36	20.9	0.0
09:37	20.9	0.0
09:38	20.9	0.0
09:39	20.9	0.0
09:40	20.9	0.0
09:41	20.9	0.0
09:42	20.9	0.0
09:43	20.9	0.0
09:44	20.9	0.0
09:45	20.9	0.0
09:46	20.9	0.0
09:47	20.9	0.0
09:48	20.9	0.0
09:49	20.9	0.0
09:50	20.9	0.0
<b>Avg</b>	<b>20.9</b>	<b>0.0</b>

---

# RUN SUMMARY

Number 2

Client: **Chemours**  
Location: **CHEMOURS**  
Source: **PPA**

Calibration 1

Project Number: **15418.002.009**  
Operator: **CMH**  
Date: **8 Jan 2019**

---

Method Conc. Units	O <sub>2</sub>	CO <sub>2</sub>
	EPA 3A %	EPA 3A %

---

Time: 07:59 to 09:50

### Run Averages

20.9      0.0

### Pre-run Bias at 07:25

Zero Bias	0.0	0.0
Span Bias	12.0	8.4
Span Gas	12.0	8.9

### Post-run Bias at 10:14

Zero Bias	0.0	0.0
Span Bias	11.9	8.4
Span Gas	12.0	8.9

Run averages corrected for the average of the pre-run and post-run bias

21.0      0.0

# BIAS AND CALIBRATION DRIFT

Number 2

Client: **Chemours**  
Location: **CHEMOURS**  
Source: **PPA**

Project Number: **15418.002.009**  
Operator: **CMH**  
Date: **8 Jan 2019**

Calibration 1

Start Time: 10:14

**O<sub>2</sub>**

Method: EPA 3A  
Span Conc. 21.0 %

---

<b>Bias Results</b>					
<b>Standard</b>	<b>Cal.</b>	<b>Bias</b>	<b>Difference</b>	<b>Error</b>	<b>Status</b>
<b>Gas</b>	<b>%</b>	<b>%</b>	<b>%</b>	<b>%</b>	
<b>Zero</b>	0.0	0.0	0.0	0.0	Pass
<b>Span</b>	12.0	11.9	-0.1	-0.5	Pass

---

<b>Calibration Drift</b>					
<b>Standard</b>	<b>Initial*</b>	<b>Final</b>	<b>Difference</b>	<b>Drift</b>	<b>Status</b>
<b>Gas</b>	<b>%</b>	<b>%</b>	<b>%</b>	<b>%</b>	
<b>Zero</b>	0.0	0.0	0.0	0.0	Pass
<b>Span</b>	12.0	11.9	-0.1	-0.5	Pass

\*Bias No. 1

---

**CO<sub>2</sub>**

Method: EPA 3A  
Span Conc. 16.6 %

---

<b>Bias Results</b>					
<b>Standard</b>	<b>Cal.</b>	<b>Bias</b>	<b>Difference</b>	<b>Error</b>	<b>Status</b>
<b>Gas</b>	<b>%</b>	<b>%</b>	<b>%</b>	<b>%</b>	
<b>Zero</b>	0.0	0.0	0.0	0.0	Pass
<b>Span</b>	8.6	8.4	-0.2	-1.2	Pass

---

<b>Calibration Drift</b>					
<b>Standard</b>	<b>Initial*</b>	<b>Final</b>	<b>Difference</b>	<b>Drift</b>	<b>Status</b>
<b>Gas</b>	<b>%</b>	<b>%</b>	<b>%</b>	<b>%</b>	
<b>Zero</b>	0.0	0.0	0.0	0.0	Pass
<b>Span</b>	8.4	8.4	0.0	0.0	Pass

\*Bias No. 1

---

# RUN DATA

Number 3

Client: **Chemours**  
Location: **CHEMOURS**  
Source: **PPA**

Calibration 1

Project Number: **15418.002.009**  
Operator: **CMH**  
Date: **8 Jan 2019**

---

Time	O <sub>2</sub> %	CO <sub>2</sub> %
<b>Start R3</b>		
10:53	20.7	0.0
10:54	20.7	0.0
10:55	20.7	0.0
10:56	20.7	0.0
10:57	20.7	0.0
10:58	20.8	0.0
10:59	20.8	0.0
11:00	20.7	0.0
11:01	20.7	0.0
11:02	20.7	0.0
11:03	20.7	0.0
11:04	20.8	0.0
11:05	20.7	0.0
11:06	20.7	0.0
11:07	20.8	0.0
11:08	20.8	0.0
11:09	20.8	0.0
11:10	20.8	0.0
11:11	20.8	0.0
11:12	20.9	0.0
11:13	20.9	0.0
11:14	20.9	0.0
11:15	20.9	0.0
11:16	20.9	0.0
11:17	20.9	0.0
11:18	20.9	0.0
11:19	20.9	0.0
11:20	20.9	0.0
11:21	20.9	0.0
11:22	20.9	0.0
11:23	20.9	0.0
11:24	20.9	0.0
11:25	20.9	0.0
11:26	20.9	0.0
11:27	20.9	0.0
11:28	20.9	0.0
11:29	20.9	0.0
11:30	20.9	0.0
11:31	20.9	0.0
11:32	20.9	0.0

---

# RUN DATA

Number 3

Client: **Chemours**  
Location: **CHEMOURS**  
Source: **PPA**

Project Number: **15418.002.009**  
Operator: **CMH**  
Date: **8 Jan 2019**

Calibration 1

---

Time	O <sub>2</sub> %	CO <sub>2</sub> %
11:33	20.9	0.0
11:34	20.9	0.0
11:35	20.9	0.0
11:36	20.9	0.0
11:37	20.9	0.0
11:38	20.9	0.0
11:39	20.9	0.0
11:40	20.9	0.0
11:41	20.9	0.0
	<b>end port 1</b>	
	<b>start port 2</b>	
12:04	20.7	0.0
12:05	20.7	0.0
12:06	20.7	0.0
12:07	20.7	0.0
12:08	20.7	0.0
12:09	20.7	0.0
12:10	20.7	0.0
12:11	20.7	0.0
12:12	20.8	0.0
12:13	20.8	0.0
12:14	20.8	0.0
12:15	20.8	0.0
12:16	20.8	0.0
12:17	20.8	0.0
12:18	20.8	0.0
12:19	20.8	0.0
12:20	20.8	0.0
12:21	20.9	0.0
12:22	20.9	0.0
12:23	20.9	0.0
12:24	20.8	0.0
12:25	20.8	0.0
12:26	20.9	0.0
12:27	20.8	0.0
12:28	20.8	0.0
12:29	20.8	0.0
12:30	20.8	0.0
12:31	20.8	0.0
12:32	20.9	0.0
12:33	20.8	0.0

# RUN DATA

Number 3

Client: **Chemours**  
Location: **CHEMOURS**  
Source: **PPA**

Project Number: **15418.002.009**  
Operator: **CMH**  
Date: **8 Jan 2019**

Calibration 1

---

Time	O <sub>2</sub> %	CO <sub>2</sub> %
12:34	20.8	0.0
12:35	20.9	0.0
12:36	20.8	0.0
12:37	20.8	0.0
12:38	20.8	0.0
12:39	20.8	0.0
12:40	20.9	0.0
12:41	20.8	0.0
12:42	20.8	0.0
12:43	20.8	0.0
12:44	20.9	0.0
12:45	20.9	0.0
12:46	20.9	0.0
12:47	20.8	0.0
12:48	20.9	0.0
12:49	20.9	0.0
12:50	20.8	0.0
12:51	20.9	0.0
12:52	20.8	0.0
12:53	20.8	0.0
12:54	20.8	0.0
12:55	20.8	0.0
<b>Avg</b>	<b>20.8</b>	<b>0.0</b>

---



# RUN SUMMARY

Number 3

Client: **Chemours**  
Location: **CHEMOURS**  
Source: **PPA**

Calibration 1

Project Number: **15418.002.009**  
Operator: **CMH**  
Date: **8 Jan 2019**

---

<b>Method</b>	<b>O<sub>2</sub></b>	<b>CO<sub>2</sub></b>
<b>Conc. Units</b>	<b>EPA 3A</b>	<b>EPA 3A</b>
	<b>%</b>	<b>%</b>

---

Time: 10:52 to 12:55

### Run Averages

20.8            0.0

### Pre-run Bias at 10:14

<b>Zero Bias</b>	0.0	0.0
<b>Span Bias</b>	11.9	8.4
<b>Span Gas</b>	12.0	8.9

### Post-run Bias at 13:10

<b>Zero Bias</b>	0.0	0.0
<b>Span Bias</b>	11.8	8.4
<b>Span Gas</b>	12.0	8.9

**Run averages corrected for the average of the pre-run and post-run bias**

21.1            0.0

# BIAS AND CALIBRATION DRIFT

Number 3

Client: **Chemours**  
Location: **CHEMOURS**  
Source: **PPA**

Project Number: **15418.002.009**  
Operator: **CMH**  
Date: **8 Jan 2019**

Calibration 1

Start Time: 13:10

**O<sub>2</sub>**

Method: EPA 3A  
Span Conc. 21.0 %

---

<b>Bias Results</b>					
<b>Standard</b>	<b>Cal.</b>	<b>Bias</b>	<b>Difference</b>	<b>Error</b>	<b>Status</b>
<b>Gas</b>	<b>%</b>	<b>%</b>	<b>%</b>	<b>%</b>	
<b>Zero</b>	0.0	0.0	0.0	0.0	Pass
<b>Span</b>	12.0	11.8	-0.2	-1.0	Pass

---

<b>Calibration Drift</b>					
<b>Standard</b>	<b>Initial*</b>	<b>Final</b>	<b>Difference</b>	<b>Drift</b>	<b>Status</b>
<b>Gas</b>	<b>%</b>	<b>%</b>	<b>%</b>	<b>%</b>	
<b>Zero</b>	0.0	0.0	0.0	0.0	Pass
<b>Span</b>	11.9	11.8	-0.1	-0.5	Pass

\*Bias No. 2

---

**CO<sub>2</sub>**

Method: EPA 3A  
Span Conc. 16.6 %

---

<b>Bias Results</b>					
<b>Standard</b>	<b>Cal.</b>	<b>Bias</b>	<b>Difference</b>	<b>Error</b>	<b>Status</b>
<b>Gas</b>	<b>%</b>	<b>%</b>	<b>%</b>	<b>%</b>	
<b>Zero</b>	0.0	0.0	0.0	0.0	Pass
<b>Span</b>	8.6	8.4	-0.2	-1.2	Pass

---

<b>Calibration Drift</b>					
<b>Standard</b>	<b>Initial*</b>	<b>Final</b>	<b>Difference</b>	<b>Drift</b>	<b>Status</b>
<b>Gas</b>	<b>%</b>	<b>%</b>	<b>%</b>	<b>%</b>	
<b>Zero</b>	0.0	0.0	0.0	0.0	Pass
<b>Span</b>	8.4	8.4	0.0	0.0	Pass

\*Bias No. 2

---

---

**APPENDIX C**  
**LABORATORY ANALYTICAL REPORT**

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Note: The complete analytical report is included on the attached CD.

## Client Sample Results

Client: Chemours Company FC, LLC The  
Project/Site: PPA Carbon Bed Outlet - M0010

TestAmerica Job ID: 140-13892-1

**Client Sample ID: G-2942,2943 PPA CARBON BED OUTLET**

**Lab Sample ID: 140-13892-1**

**R1 M0010 FH**

Date Collected: 01/07/19 00:00

Matrix: Air

Date Received: 01/09/19 11:25

Sample Container: Air Train

**Method: 8321A - PFOA and PFOS**

Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
HFPO-DA	3.85		0.101	0.0109	ug/Sample		01/10/19 08:39	01/17/19 11:26	1
Surrogate	%Recovery	Qualifier	Limits						
13C3 HFPO-DA	120		50 - 200						
							Prepared	Analyzed	Dil Fac
							01/10/19 08:39	01/17/19 11:26	1

**Client Sample ID: G-2944,2945,2947 PPA CARBON BED**

**Lab Sample ID: 140-13892-2**

**OUTLET R1 M0010 BH**

Date Collected: 01/07/19 00:00

Matrix: Air

Date Received: 01/09/19 11:25

Sample Container: Air Train

**Method: 8321A - PFOA and PFOS**

Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
HFPO-DA	0.0956	J	0.200	0.0400	ug/Sample		01/09/19 11:32	01/17/19 10:31	1
Surrogate	%Recovery	Qualifier	Limits						
13C3 HFPO-DA	83		50 - 200						
							Prepared	Analyzed	Dil Fac
							01/09/19 11:32	01/17/19 10:31	1

**Client Sample ID: G-2946 PPA CARBON BED OUTLET R1**

**Lab Sample ID: 140-13892-3**

**M0010 IMP 1,2&3 CONDENSATE**

Date Collected: 01/07/19 00:00

Matrix: Air

Date Received: 01/09/19 11:25

Sample Container: Air Train

**Method: 8321A - HFPO-DA**

Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
HFPO-DA	ND		0.190	0.00969	ug/Sample		01/10/19 08:41	01/17/19 11:49	1
Surrogate	%Recovery	Qualifier	Limits						
13C3 HFPO-DA	96		50 - 200						
							Prepared	Analyzed	Dil Fac
							01/10/19 08:41	01/17/19 11:49	1

**Client Sample ID: G-2948 PPA CARBON BED OUTLET R1**

**Lab Sample ID: 140-13892-4**

**M0010 BREAKTHROUGH XAD-2 RESIN TUBE**

Date Collected: 01/07/19 00:00

Matrix: Air

Date Received: 01/09/19 11:25

Sample Container: Air Train

**Method: 8321A - PFOA and PFOS**

Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
HFPO-DA	0.0489	J	0.200	0.0400	ug/Sample		01/09/19 11:32	01/17/19 10:34	1
Surrogate	%Recovery	Qualifier	Limits						
13C3 HFPO-DA	90		50 - 200						
							Prepared	Analyzed	Dil Fac
							01/09/19 11:32	01/17/19 10:34	1

TestAmerica Knoxville

## Client Sample Results

Client: Chemours Company FC, LLC The  
Project/Site: PPA Carbon Bed Outlet - M0010

TestAmerica Job ID: 140-13892-1

**Client Sample ID: G-2949,2950 PPA CARBON BED OUTLET  
R2 M0010 FH**

**Lab Sample ID: 140-13892-5**

Date Collected: 01/08/19 00:00

Matrix: Air

Date Received: 01/09/19 11:25

Sample Container: Air Train

Method: 8321A - PFOA and PFOS

Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
HFPO-DA	3.40		0.151	0.0163	ug/Sample		01/10/19 08:39	01/17/19 11:29	1
Surrogate	%Recovery	Qualifier	Limits				Prepared	Analyzed	Dil Fac
13C3 HFPO-DA	121		50 - 200				01/10/19 08:39	01/17/19 11:29	1

**Client Sample ID: G-2951,2952,2954 PPA CARBON BED  
OUTLET R2 M0010 BH**

**Lab Sample ID: 140-13892-6**

Date Collected: 01/08/19 00:00

Matrix: Air

Date Received: 01/09/19 11:25

Sample Container: Air Train

Method: 8321A - PFOA and PFOS

Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
HFPO-DA	0.556		0.250	0.0500	ug/Sample		01/09/19 11:32	01/17/19 10:37	1
Surrogate	%Recovery	Qualifier	Limits				Prepared	Analyzed	Dil Fac
13C3 HFPO-DA	92		50 - 200				01/09/19 11:32	01/17/19 10:37	1

**Client Sample ID: G-2953 PPA CARBON BED OUTLET R2  
M0010 IMP 1,2&3 CONDENSATE**

**Lab Sample ID: 140-13892-7**

Date Collected: 01/08/19 00:00

Matrix: Air

Date Received: 01/09/19 11:25

Sample Container: Air Train

Method: 8321A - HFPO-DA

Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
HFPO-DA	ND		0.205	0.0105	ug/Sample		01/10/19 08:41	01/17/19 11:52	1
Surrogate	%Recovery	Qualifier	Limits				Prepared	Analyzed	Dil Fac
13C3 HFPO-DA	96		50 - 200				01/10/19 08:41	01/17/19 11:52	1

**Client Sample ID: G-2955 PPA CARBON BED OUTLET R2  
M0010 BREAKTHROUGH XAD-2 RESIN TUBE**

**Lab Sample ID: 140-13892-8**

Date Collected: 01/08/19 00:00

Matrix: Air

Date Received: 01/09/19 11:25

Sample Container: Air Train

Method: 8321A - PFOA and PFOS

Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
HFPO-DA	0.276		0.200	0.0400	ug/Sample		01/09/19 11:32	01/17/19 10:41	1
Surrogate	%Recovery	Qualifier	Limits				Prepared	Analyzed	Dil Fac
13C3 HFPO-DA	89		50 - 200				01/09/19 11:32	01/17/19 10:41	1

TestAmerica Knoxville

## Client Sample Results

Client: Chemours Company FC, LLC The  
Project/Site: PPA Carbon Bed Outlet - M0010

TestAmerica Job ID: 140-13892-1

**Client Sample ID: G-2956,2957 PPA CARBON BED OUTLET R3 M0010 FH**

**Lab Sample ID: 140-13892-9**

Date Collected: 01/08/19 00:00

Matrix: Air

Date Received: 01/09/19 11:25

Sample Container: Air Train

**Method: 8321A - PFOA and PFOS**

Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
HFPO-DA	3.24		0.126	0.0136	ug/Sample		01/10/19 08:39	01/17/19 11:32	1
Surrogate	%Recovery	Qualifier	Limits				Prepared	Analyzed	Dil Fac
13C3 HFPO-DA	122		50 - 200				01/10/19 08:39	01/17/19 11:32	1

**Client Sample ID: G-2958,2959,2961 PPA CARBON BED OUTLET R3 M0010 BH**

**Lab Sample ID: 140-13892-10**

Date Collected: 01/08/19 00:00

Matrix: Air

Date Received: 01/09/19 11:25

Sample Container: Air Train

**Method: 8321A - PFOA and PFOS**

Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
HFPO-DA	0.105	J	0.225	0.0450	ug/Sample		01/09/19 11:32	01/17/19 10:44	1
Surrogate	%Recovery	Qualifier	Limits				Prepared	Analyzed	Dil Fac
13C3 HFPO-DA	89		50 - 200				01/09/19 11:32	01/17/19 10:44	1

**Client Sample ID: G-2960 PPA CARBON BED OUTLET R3 M0010 IMP 1,2&3 CONDENSATE**

**Lab Sample ID: 140-13892-11**

Date Collected: 01/08/19 00:00

Matrix: Air

Date Received: 01/09/19 11:25

Sample Container: Air Train

**Method: 8321A - HFPO-DA**

Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
HFPO-DA	0.207	J	0.210	0.0107	ug/Sample		01/10/19 08:41	01/17/19 11:55	1
Surrogate	%Recovery	Qualifier	Limits				Prepared	Analyzed	Dil Fac
13C3 HFPO-DA	102		50 - 200				01/10/19 08:41	01/17/19 11:55	1

**Client Sample ID: G-2962 PPA CARBON BED OUTLET R3 M0010 BREAKTHROUGH XAD-2 RESIN TUBE**

**Lab Sample ID: 140-13892-12**

Date Collected: 01/08/19 00:00

Matrix: Air

Date Received: 01/09/19 11:25

Sample Container: Air Train

**Method: 8321A - PFOA and PFOS**

Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
HFPO-DA	ND		0.200	0.0400	ug/Sample		01/09/19 11:32	01/17/19 10:47	1
Surrogate	%Recovery	Qualifier	Limits				Prepared	Analyzed	Dil Fac
13C3 HFPO-DA	89		50 - 200				01/09/19 11:32	01/17/19 10:47	1

TestAmerica Knoxville

## Client Sample Results

Client: Chemours Company FC, LLC The  
Project/Site: PPA Carbon Bed Outlet QC Samples

TestAmerica Job ID: 140-13893-1

**Client Sample ID: C-2401,2402 PPA CARBON BED QC M0010  
FH BT**

**Lab Sample ID: 140-13893-1**

Date Collected: 01/08/19 00:00  
Date Received: 01/09/19 11:25  
Sample Container: Air Train

Matrix: Air

Method: 8321A - PFOA and PFOS

Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
HFPO-DA	0.0356		0.0260	0.00281	ug/Sample		01/10/19 08:39	01/17/19 11:36	1
Surrogate	%Recovery	Qualifier	Limits				Prepared	Analyzed	Dil Fac
13C3 HFPO-DA	101		50 - 200				01/10/19 08:39	01/17/19 11:36	1

**Client Sample ID: C-2403,2404,2406 PPA CARBON BED QC  
M0010 BH BT**

**Lab Sample ID: 140-13893-2**

Date Collected: 01/08/19 00:00  
Date Received: 01/09/19 11:25  
Sample Container: Air Train

Matrix: Air

Method: 8321A - PFOA and PFOS

Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
HFPO-DA	0.121	J	0.200	0.0400	ug/Sample		01/09/19 11:32	01/17/19 10:50	1
Surrogate	%Recovery	Qualifier	Limits				Prepared	Analyzed	Dil Fac
13C3 HFPO-DA	91		50 - 200				01/09/19 11:32	01/17/19 10:50	1

**Client Sample ID: C-2405 PPA CARBON BED QC M0010 IMP  
1,2&3 CONDENSATE BT**

**Lab Sample ID: 140-13893-3**

Date Collected: 01/08/19 00:00  
Date Received: 01/09/19 11:25  
Sample Container: Air Train

Matrix: Air

Method: 8321A - HFPO-DA

Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
HFPO-DA	ND		0.00250	0.000128	ug/Sample		01/10/19 08:41	01/17/19 11:59	1
Surrogate	%Recovery	Qualifier	Limits				Prepared	Analyzed	Dil Fac
13C3 HFPO-DA	106		50 - 200				01/10/19 08:41	01/17/19 11:59	1

**Client Sample ID: C-2407 PPA CARBON BED QC M0010  
BREAKTHROUGH XAD-2 RESIN TUBE BT**

**Lab Sample ID: 140-13893-4**

Date Collected: 01/08/19 00:00  
Date Received: 01/09/19 11:25  
Sample Container: Air Train

Matrix: Air

Method: 8321A - PFOA and PFOS

Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
HFPO-DA	ND		0.200	0.0400	ug/Sample		01/09/19 11:32	01/17/19 10:53	1
Surrogate	%Recovery	Qualifier	Limits				Prepared	Analyzed	Dil Fac
13C3 HFPO-DA	91		50 - 200				01/09/19 11:32	01/17/19 10:53	1

TestAmerica Knoxville

## Client Sample Results

Client: Chemours Company FC, LLC The  
Project/Site: PPA Carbon Bed Outlet QC Samples

TestAmerica Job ID: 140-13893-1

**Client Sample ID: C-2408 PPA CARBON BED QC M0010 DI  
WATER RB**

**Lab Sample ID: 140-13893-5**

Date Collected: 01/07/19 00:00  
Date Received: 01/09/19 11:25  
Sample Container: Air Train

Matrix: Air

Method: 8321A - HFPO-DA

Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
HFPO-DA	ND		0.00250	0.000128	ug/Sample		01/10/19 08:41	01/17/19 12:02	1
Surrogate	%Recovery	Qualifier	Limits				Prepared	Analyzed	Dil Fac
13C3 HFPO-DA	130		50 - 200				01/10/19 08:41	01/17/19 12:02	1

**Client Sample ID: C-2409 PPA CARBON BED QC M0010 MEOH  
WITH 5% NH4OH RB**

**Lab Sample ID: 140-13893-6**

Date Collected: 01/07/19 00:00  
Date Received: 01/09/19 11:25  
Sample Container: Air Train

Matrix: Air

Method: 8321A - PFOA and PFOS

Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
HFPO-DA	ND		0.0250	0.00500	ug/Sample		01/09/19 11:32	01/17/19 11:00	1
Surrogate	%Recovery	Qualifier	Limits				Prepared	Analyzed	Dil Fac
13C3 HFPO-DA	100		50 - 200				01/09/19 11:32	01/17/19 11:00	1

**Client Sample ID: C-2410 PPA CARBON BED QC M0010 XAD-2  
RESIN TUBE RB**

**Lab Sample ID: 140-13893-7**

Date Collected: 01/07/19 00:00  
Date Received: 01/09/19 11:25  
Sample Container: Air Train

Matrix: Air

Method: 8321A - PFOA and PFOS

Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
HFPO-DA	ND		0.200	0.0400	ug/Sample		01/09/19 11:32	01/17/19 11:03	1
Surrogate	%Recovery	Qualifier	Limits				Prepared	Analyzed	Dil Fac
13C3 HFPO-DA	95		50 - 200				01/09/19 11:32	01/17/19 11:03	1

**Client Sample ID: C-2411 PPA CARBON BED QC M0010 MEOH  
WITH 5% NH4OH TB**

**Lab Sample ID: 140-13893-8**

Date Collected: 01/07/19 00:00  
Date Received: 01/09/19 11:25  
Sample Container: Air Train

Matrix: Air

Method: 8321A - PFOA and PFOS

Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
HFPO-DA	ND		0.0250	0.00500	ug/Sample		01/09/19 11:32	01/17/19 11:06	1
Surrogate	%Recovery	Qualifier	Limits				Prepared	Analyzed	Dil Fac
13C3 HFPO-DA	116		50 - 200				01/09/19 11:32	01/17/19 11:06	1

TestAmerica Knoxville



## Client Sample Results

Client: Chemours Company FC, LLC The  
 Project/Site: PPA Carbon Bed Outlet QC Samples

TestAmerica Job ID: 140-13893-1

**Client Sample ID: C-2412 PPA CARBON BED QC M0010 XAD-2**

**Lab Sample ID: 140-13893-9**

**RESIN TUBE TB**

Date Collected: 01/07/19 00:00

Matrix: Air

Date Received: 01/09/19 11:25

Sample Container: Air Train

Method: 8321A - PFOA and PFOS										
Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac	
HFPO-DA	ND		0.200	0.0400	ug/Sample		01/09/19 11:32	01/17/19 11:10	1	
Surrogate	%Recovery	Qualifier	Limits				Prepared	Analyzed	Dil Fac	
13C3 HFPO-DA	94		50 - 200				01/09/19 11:32	01/17/19 11:10	1	

**Client Sample ID: C-2413 PPA CARBON BED QC M0010**

**Lab Sample ID: 140-13893-10**

**COMBINED GLASSWARE RINSES (MEOH/5% NH4OH) PB**

Date Collected: 01/07/19 00:00

Matrix: Air

Date Received: 01/09/19 11:25

Sample Container: Air Train

Method: 8321A - PFOA and PFOS										
Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac	
HFPO-DA	0.0248	J	0.0250	0.00500	ug/Sample		01/09/19 11:32	01/17/19 11:13	1	
Surrogate	%Recovery	Qualifier	Limits				Prepared	Analyzed	Dil Fac	
13C3 HFPO-DA	114		50 - 200				01/09/19 11:32	01/17/19 11:13	1	

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**APPENDIX D**  
**SAMPLE CALCULATIONS**

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**SAMPLE CALCULATIONS FOR  
HFPO DIMER ACID (METHOD 0010)**

**Client: Chemours**  
**Test Number: Run 3**  
**Test Location: PPA Stack**

**Plant: Fayetteville, NC**  
**Test Date: 01/08/19**  
**Test Period: 1053-1255**

**1. HFPO Dimer Acid concentration, lbs/dscf.**

$$\text{Conc1} = \frac{W \times 2.2046 \times 10^{-9}}{V_m(\text{std})}$$

$$\text{Conc1} = \frac{3.6 \times 2.2046 \times 10^{-9}}{43.038}$$

$$\text{Conc1} = 1.82\text{E-}10$$

Where:

W = Weight of HFPO Dimer Acid collected in sample in ug.

Conc1 = Division Stack HFPO Dimer Acid concentration, lbs/dscf.

$2.2046 \times 10^{-9}$  = Conversion factor from ug to lbs.

**2. HFPO Dimer Acid concentration, ug/dscm.**

$$\text{Conc2} = W / (V_m(\text{std}) \times 0.02832)$$

$$\text{Conc2} = 3.6 / (43.038 \times 0.02832)$$

$$\text{Conc2} = 2.91\text{E+}00$$

Where:

Conc2 = Division Stack HFPO Dimer Acid concentration, ug/dscm.

0.02832 = Conversion factor from cubic feet to cubic meters.

**3. HFPO Dimer Acid mass emission rate, lbs/hr.**

$$MR1_{(Outlet)} = \text{Conc1} \times Qs(\text{std}) \times 60 \text{ min/hr}$$

$$MR1_{(Outlet)} = 1.82\text{E-}10 \times 10470 \times 60$$

$$MR1_{(Outlet)} = 1.14\text{E-}04$$

Where:

$$MR1_{(Outlet)} = \text{Division Stack HFPO Dimer Acid mass emission rate, lbs/hr.}$$

**4. HFPO Dimer Acid mass emission rate, g/sec.**

$$MR2_{(Outlet)} = \text{PMR1} \times 453.59 / 3600$$

$$MR2_{(Outlet)} = 1.14\text{E-}04 \times 453.59 / 3600$$

$$MR2_{(Outlet)} = 1.44\text{E-}05$$

Where:

$$MR2_{(Outlet)} = \text{Division Stack HFPO Dimer Acid mass emission rate, g/sec.}$$

$$453.6 = \text{Conversion factor from pounds to grams.}$$

$$3600 = \text{Conversion factor from hours to seconds.}$$

**EXAMPLE CALCULATIONS FOR  
VOLUMETRIC FLOW AND MOISTURE AND ISOKINETICS**

Client: Chemours  
Test Number: Run 3  
Test Location: PPA Stack

Facility: Fayetteville, NC  
Test Date: 1/08/19  
Test Period: 1053-1255

**1. Volume of dry gas sampled at standard conditions (68 deg F, 29.92 in. Hg), dscf.**

$$Vm(std) = \frac{17.64 \times Y \times Vm \times \left( Pb + \frac{\Delta H}{13.6} \right)}{(Tm + 460)}$$

$$Vm(std) = \frac{17.64 \times 0.9915 \times 42.900 \times \left( 30.08 + \frac{0.622}{13.6} \right)}{65.21 + 460} = 43.038$$

Where:

$Vm(std)$  = Volume of gas sample measured by the dry gas meter, corrected to standard conditions, dscf.  
 $Vm$  = Volume of gas sample measured by the dry gas meter at meter conditions, dcf.  
 $Pb$  = Barometric Pressure, in Hg.  
 $\Delta H$  = Average pressure drop across the orifice meter, in H<sub>2</sub>O  
 $Tm$  = Average dry gas meter temperature, deg F.  
 $Y$  = Dry gas meter calibration factor.  
 $17.64$  = Factor that includes ratio of standard temperature (528 deg R) to standard pressure (29.92 in. Hg), deg R/in. Hg.  
 $13.6$  = Specific gravity of mercury.

**2. Volume of water vapor in the gas sample corrected to standard conditions, scf.**

$$Vw(std) = (0.04707 \times Vwc) + (0.04715 \times Wwsg)$$

$$Vw(std) = (0.04707 \times 14.0) + (0.04715 \times 11.2) = 1.19$$

Where:

$Vw(std)$  = Volume of water vapor in the gas sample corrected to standard conditions, scf.  
 $Vwc$  = Volume of liquid condensed in impingers, ml.  
 $Wwsg$  = Weight of water vapor collected in silica gel, g.  
 $0.04707$  = Factor which includes the density of water (0.002201 lb/ml), the molecular weight of water (18.0 lb/lb-mole), the ideal gas constant 21.85 (in. Hg) (ft<sup>3</sup>/lb-mole)(deg R); absolute temperature at standard conditions (528 deg R), absolute pressure at standard conditions (29.92 in. Hg), ft<sup>3</sup>/ml.  
 $0.04715$  = Factor which includes the molecular weight of water (18.0 lb/lb-mole), the ideal gas constant 21.85 (in. Hg) (ft<sup>3</sup>/lb-mole)(deg R); absolute temperature at standard conditions (528 deg R), absolute pressure at standard conditions (29.92 in. Hg), and 453.6 g/lb, ft<sup>3</sup>/g.

### 3. Moisture content

$$\text{bws} = \frac{V_w(\text{std})}{V_w(\text{std}) + V_m(\text{std})}$$
$$\text{bws} = \frac{1.19}{1.19 + 43.038} = 0.027$$

Where:

bws = Proportion of water vapor, by volume, in the gas stream, dimensionless.

### 4. Mole fraction of dry gas.

$$\text{Md} = 1 - \text{bws}$$
$$\text{Md} = 1 - 0.027 = 0.973$$

Where:

Md = Mole fraction of dry gas, dimensionless.

### 5. Dry molecular weight of gas stream, lb/lb-mole.

$$\text{MWd} = (0.440 \times \% \text{CO}_2) + (0.320 \times \% \text{O}_2) + (0.280 \times (\% \text{N}_2 + \% \text{CO}))$$
$$\text{MWd} = (0.440 \times 0.0) + (0.320 \times 20.9) + (0.280 \times (79.1 + 0.0))$$
$$\text{MWd} = 28.84$$

Where:

MWd = Dry molecular weight, lb/lb-mole.  
% CO<sub>2</sub> = Percent carbon dioxide by volume, dry basis.  
% O<sub>2</sub> = Percent oxygen by volume, dry basis.  
% N<sub>2</sub> = Percent nitrogen by volume, dry basis.  
% CO = Percent carbon monoxide by volume, dry basis.  
0.440 = Molecular weight of carbon dioxide, divided by 100.  
0.320 = Molecular weight of oxygen, divided by 100.  
0.280 = Molecular weight of nitrogen or carbon monoxide, divided by 100.

### 6. Actual molecular weight of gas stream (wet basis), lb/lb-mole.

$$\text{MWs} = (\text{MWd} \times \text{Md}) + (18 \times (1 - \text{Md}))$$
$$\text{MWs} = (28.84 \times 0.973) + (18 \times (1 - 0.973)) = 28.55$$

Where:

MWs = Molecular weight of wet gas, lb/lb-mole.  
18 = Molecular weight of water, lb/lb-mole.

**7. Average velocity of gas stream at actual conditions, ft/sec.**

$$V_s = 85.49 \times C_p \times ((\Delta p)^{1/2})_{\text{avg}} \times \left( \frac{T_s (\text{avg})}{P_s \times MW_s} \right)^{1/2}$$

$$V_s = 85.49 \times 0.84 \times 0.64656 \times \left( \frac{528}{30.10 \times 28.55} \right)^{1/2} = 36.4$$

Where:

- $V_s$  = Average gas stream velocity, ft/sec.
- 85.49 = Pitot tube constant, ft/sec  $\times \frac{(\text{lb/lb-mole})(\text{in. Hg})^{1/2}}{(\text{deg R})(\text{in H}_2\text{O})}$
- $C_p$  = Pitot tube coefficient, dimensionless.
- $T_s$  = Absolute gas stream temperature, deg R =  $T_s$ , deg F + 460.
- $P_s$  = Absolute gas stack pressure, in. Hg. =  $P_b + \frac{P(\text{static})}{13.6}$
- $\Delta p$  = Velocity head of stack, in. H<sub>2</sub>O.

**8. Average gas stream volumetric flow rate at actual conditions, wacf/min.**

$$Q_s(\text{act}) = 60 \times V_s \times A_s$$

$$Q_s(\text{act}) = 60 \times 36.4 \times 4.90 = 10703$$

Where:

- $Q_s(\text{act})$  = Volumetric flow rate of wet stack gas at actual conditions, wacf/min.
- $A_s$  = Cross-sectional area of stack, ft<sup>2</sup>.
- 60 = Conversion factor from seconds to minutes.

**9. Average gas stream dry volumetric flow rate at standard conditions, dscf/min.**

$$Q_s(\text{std}) = 17.64 \times M_d \times \frac{P_s}{T_s} \times Q_s(\text{act})$$

$$Q_s(\text{std}) = 17.64 \times 0.973 \times \frac{30.10}{528.1} \times 10703$$

$$Q_s(\text{std}) = 10470$$

Where:

- $Q_s(\text{std})$  = Volumetric flow rate of dry stack gas at standard conditions, dscf/min.

**10. Isokinetic variation calculated from intermediate values, percent.**

$$I = \frac{17.327 \times T_s \times V_m(\text{std})}{V_s \times O \times P_s \times M_d \times (D_n)^2}$$

$$I = \frac{17.327 \times 528 \times 43.038}{36.4 \times 96 \times 30.10 \times 0.973 \times (0.190)^2} = 106.6$$

Where:

- I = Percent of isokinetic sampling.
- O = Total sampling time, minutes.
- D<sub>n</sub> = Diameter of nozzle, inches.
- 17.327 = Factor which includes standard temperature (528 deg R), standard pressure (29.92 in. Hg), the formula for calculating area of circle  $D^{2/4}$ , conversion of square feet to square inches (144), conversion of seconds to minutes (60), and conversion to percent (100),  $\frac{(\text{in. Hg})(\text{in}^2)(\text{min})}{(\text{deg R})(\text{ft}^2)(\text{sec})}$



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**APPENDIX E**  
**EQUIPMENT CALIBRATION RECORDS**

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Balance ID:

Date	Initials	Calibration Weight	Measured Weight <sup>(1)</sup>	Maintenance and Adjustments
10/30/17	MPW	500.0	499.8	
10/31/17	MPW	500.0	499.9	
9/5/18	CH	500.0	500.1	
9/13/18	ZA	500.0	500.1	
10/8/18	JDO	500	499.6	NA - SOC
10/9/18	JDO	500	499.7	NA - SOC
10/10/18	JMO	500	499.6	NA - SOC
10/11/18	JMO	500	499.7	NA - SOC
10/23/18	TB	500	499.8	NA - Chem CW
10/24/18	JDO	500	499.0	NA Chem CW
10/25/18	JMO	500	499.8	NA Chem CW
01/07/19	CH	500	499.7	NA Chemours
01/08/19	CH	500	499.7	NA Chemours
01/22/19	CH	500	499.7	NA Chemours
1/16/19	JDO	500	499.6	NA Chem
1/18/19	CW	500.0	499.8	NA Chemours

Weight must be within ± 0.5 grams of calibration weight

## Long Cal and Temperature Cal Datasheet for Standard Dry Gas Meter Console

Calibrator PM

Meter Box Number 21

Ambient Temp 71

Date 12-Feb-18

Wet Test Meter Number P-2952

Temp Reference Source Thermocouple Simulator  
(Accuracy +/- 1°F)

Dry Gas Meter Number 17485140

Setting	Gas Volume		Temperatures				Time, min (O)	Baro Press, in Hg ( Pb)	29.64
	Wet Test Meter	Dry gas Meter	Wet Test Meter	Dry Gas Meter				Calibration Results	
in H <sub>2</sub> O (ΔH)	ft <sup>3</sup> (Vw)	ft <sup>3</sup> (Vd)	°F (Tw)	Outlet, °F (Tdo)	Inlet, °F (Tdi)	Average, °F (Td)		Y	ΔH
0.5	5.0	570.015	70.0	69.00	69.00	70.0	13.00	0.9948	1.9159
		575.035		71.00	71.00				
		5.020		70.00	70.00				
1.0	5.0	575.035	70.0	71.00	71.00	71.5	9.3	0.9910	1.9555
		580.082		72.00	72.00				
		5.047		71.50	71.50				
1.5	10.0	580.082	70.0	72.00	72.00	73.0	15.6	0.9898	2.0575
		590.205		74.00	74.00				
		10.123		73.00	73.00				
2.0	10.0	590.205	70.0	74.00	74.00	74.5	13.6	0.9945	2.0792
		600.296		75.00	75.00				
		10.091		74.50	74.50				
3.0	10.0	600.296	70.0	75.00	75.00	75.5	11.0	0.9873	2.0365
		610.454		76.00	76.00				
		10.158		75.50	75.50				
<b>Average</b>								<b>0.9915</b>	<b>2.0089</b>

Vw - Gas Volume passing through the wet test meter  
 Vd - Gas Volume passing through the dry gas meter  
 Tw - Temp of gas in the wet test meter  
 Tdi - Temp of the inlet gas of the dry gas meter  
 Tdo - Temp of the outlet gas of the dry gas meter  
 Td - Average temp of the gas in the dry gas meter

O - Time of calibration run  
 Pb - Barometric Pressure  
 ΔH - Pressure differential across orifice  
 Y - Ratio of accuracy of wet test meter to dry gas meter

$$Y = \frac{Vw * Pb * (td + 460)}{Vd * \left[ Pb + \frac{(\Delta H)}{13.6} \right] * (tw + 460)}$$

$$\Delta H = \left[ \frac{0.0317 * \Delta H}{Pb * (td + 460)} \right] * \left[ \frac{(tw + 460) * O}{Vw} \right]^2$$

Reference Temperature	Temperature Reading from Individual Thermocouple Input <sup>1</sup>						Average Temperature Reading	Temp Difference <sup>2</sup> (%)
	Channel Number							
	1	2	3	4	5	6		
Select Temperature <input type="radio"/> °C <input checked="" type="radio"/> °F								
32	32	32	32	32	32	32.0	0.0%	
212	212	212	212	212	212	212.0	0.0%	
932	932	932	932	932	932	932.0	0.0%	
1832	1830	1830	1830	1830	1830	1830.0	0.1%	

<sup>1</sup> - Channel Temps must agree with +/- 5°F or 3°C

<sup>2</sup> - Acceptable Temperature Difference less than 1.5 %

$$\text{Temp Diff} = \left[ \frac{(\text{Reference Temp}^{\circ\text{F}} + 460) - (\text{Test Temp}^{\circ\text{F}} + 460)}{\text{Reference Temp}^{\circ\text{F}} + 460} \right]$$

**Y Factor Calibration Check Calculation**  
**MODIFIED METHOD 0010 TEST TRAIN**  
**PPA STACK**  
**METER BOX NO. 21**  
**01/07/2019 + 01/08/2019**

	Run 1	Run 2	Run 3
MWd = Dry molecular weight source gas, lb/lb-mole.			
0.32 = Molecular weight of oxygen, divided by 100.			
0.44 = Molecular weight of carbon dioxide, divided by 100.			
0.28 = Molecular weight of nitrogen or carbon monoxide, divided by 100.			
% CO <sub>2</sub> = Percent carbon dioxide by volume, dry basis.	0.0	0.0	0.0
% O <sub>2</sub> = Percent oxygen by volume, dry basis.	20.9	20.9	20.9

$$MWd = (0.32 * O_2) + (0.44 * CO_2) + (0.28 * (100 - (CO_2 + O_2)))$$

$$MWd = (0.32 * 20.9) + (0.44 * 0) + (0.28 * (100 - (0 + 20.9)))$$

$$MWd = (6.69) + (0.00) + (22.15)$$

<b>MWd =</b>	28.84	28.84	28.84
--------------	-------	-------	-------

Tma = Source Temperature, absolute(°R)			
Tm = Average dry gas meter temperature, deg F.	65.8	51.5	65.2

$$Tma = Ts + 460$$

$$Tma = 65.75 + 460$$

<b>Tma =</b>	525.75	511.46	525.21
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Ps = Absolute meter pressure, inches Hg.			
13.60 = Specific gravity of mercury.			
delta H = Avg pressure drop across the orifice meter during sampling, in H <sub>2</sub> O	0.71	0.59	0.62
Pb = Barometric Pressure, in Hg.	30.40	30.08	30.08

$$Pm = Pb + (\text{delta H} / 13.6)$$

$$Pm = 30.4 + (0.7120833333333334 / 13.6)$$

<b>Pm =</b>	30.45	30.12	30.13
-------------	-------	-------	-------

Yqa = dry gas meter calibration check value, dimensionless.			
0.03 = (29.92/528)(0.75) <sup>2</sup> (in. Hg/°R) cfm <sup>2</sup> .			
29.00 = dry molecular weight of air, lb/lb-mole.			
Vm = Volume of gas sample measured by the dry gas meter at meter conditions, dcf.	44.005	40.425	42.900
Y = Dry gas meter calibration factor (based on full calibration)	0.9915	0.9915	0.9915
Delta H@ = Dry Gas meter orifice calibration coefficient, in. H <sub>2</sub> O.	2.0089	2.0089	2.0089
avg SQRT Delta H = Avg SQRT press. drop across the orifice meter during sampling, in. H <sub>2</sub> O	0.8403	0.7692	0.7870
O = Total sampling time, minutes.	96	96	96

$$Yqa = (O / Vm) * \text{SQRT} (0.0319 * Tma * 29) / (\text{Delta H}@ * Pm * MWd) * \text{avg SQRT Delta H}$$

$$Yqa = (96.00 / 44.01) * \text{SQRT} (0.0319 * 525.75 * 29) / (2.01 * 30.45 * 28.84) * 0.84$$

$$Yqa = 2.182 * \text{SQRT} 486.371 / 1,763.927 * 0.84$$

<b>Yqa =</b>	0.9626	0.9512	0.9291
--------------	--------	--------	--------

Diff = Absolute difference between Yqa and Y	2.91	4.06	6.29
--	------	------	------

$$\text{Diff} = ((Y - Yqa) / Y) * 100$$

$$\text{Diff} = ((0.9915 - 0.963) / 0.9915) * 100$$

**Average Diff = 4.42**

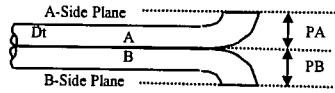
**Allowable = 5.0**

# Type S Pitot Tube Inspection Data Form

Pitot Tube Identification Number: P-696

If all Criteria PASS  
Cp is equal to 0.84

Inspection Date 1/5/18 Individual Conducting Inspection PM



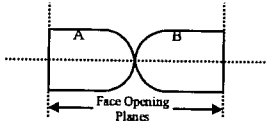
Distance to A Plane (PA) - inches 0.46  
 Distance to B Plane (PB) - inches 0.46  
 Pitot OD (Dt) - inches 0.375

**PASS/FAIL**

PASS  
PASS

$1.05 D_t < P < 1.5 D_t$

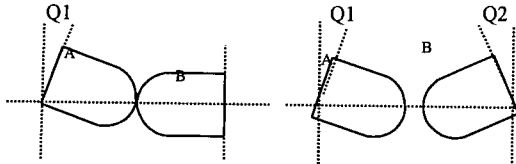
PA must Equal PB



Are Open Faces Aligned  
Perpendicular to the Tube Axis

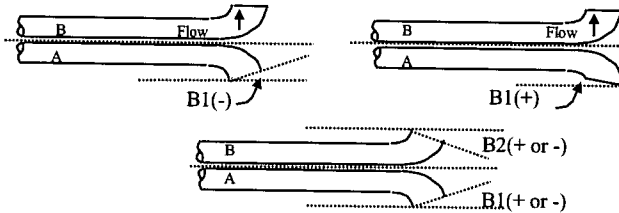
YES  NO

PASS



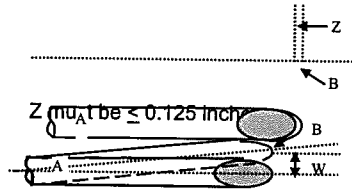
Angle of Q1 from vertical A Tube-  
degrees (absolute) 0 PASS  
 Angle of Q2 from vertical B Tube-  
degrees (absolute) 0 PASS

Q1 and Q2 must be  $\leq 10^\circ$



Angle of B1 from  
vertical A Tube-  
degrees (absolute) 0 PASS  
 Angle of B1 from  
vertical B Tube-  
degrees (absolute) 0 PASS

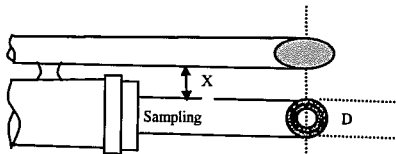
B1 or B2 must be  $\leq 5^\circ$



Horizontal offset between A and  
B Tubes (Z) - inches 0.005 PASS

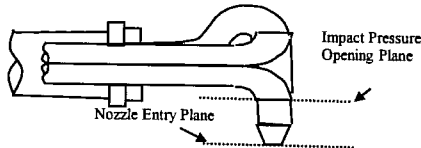
Vertical offset between A and B  
Tubes (W) - inches 0.014 PASS

W must be  $\leq 0.03125$  inches



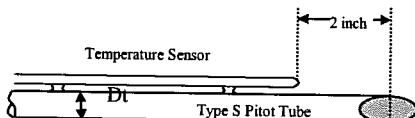
Distance between Sample  
Nozzle and Pitot (X) - inches 0.8 PASS

X must be  $\geq 0.75$  inches



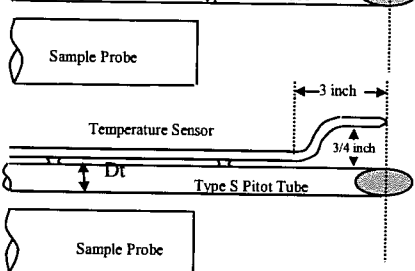
Impact Pressure  
Opening Plane is  
above the Nozzle  
Entry Plane

YES  NO  
 NA



Thermocouple meets  
the Distance Criteria  
in the adjacent figure

YES  NO  
 NA



Thermocouple meets  
the Distance Criteria  
in the adjacent figure

YES  NO  
 NA

# CERTIFICATE OF ANALYSIS

## Grade of Product: EPA Protocol

Part Number:	E03NI79E15A00E4	Reference Number:	82-401288926-1
Cylinder Number:	CC18055	Cylinder Volume:	150.5 CF
Laboratory:	124 - Riverton (SAP) - NJ	Cylinder Pressure:	2015 PSIG
PGVP Number:	B52018	Valve Outlet:	590
Gas Code:	CO2,O2,BALN	Certification Date:	Sep 04, 2018

**Expiration Date: Sep 04, 2026**

Certification performed in accordance with "EPA Traceability Protocol for Assay and Certification of Gaseous Calibration Standards (May 2012)" document EPA 600/R-12/531, using the assay procedures listed. Analytical Methodology does not require correction for analytical interference. This cylinder has a total analytical uncertainty as stated below with a confidence level of 95%. There are no significant impurities which affect the use of this calibration mixture. All concentrations are on a volume/volume basis unless otherwise noted.

Do Not Use This Cylinder below 100 psig, i.e. 0.7 megapascals.

ANALYTICAL RESULTS					
Component	Requested Concentration	Actual Concentration	Protocol Method	Total Relative Uncertainty	Assay Dates
CARBON DIOXIDE	9.000 %	8.864 %	G1	+/- 0.7% NIST Traceable	09/04/2018
OXYGEN	12.00 %	12.00 %	G1	+/- 0.4% NIST Traceable	09/04/2018
NITROGEN	Balance			-	

CALIBRATION STANDARDS					
Type	Lot ID	Cylinder No	Concentration	Uncertainty	Expiration Date
NTRM	13060629	CC413730	13.359 % CARBON DIOXIDE/NITROGEN	+/- 0.6%	May 09, 2019

ANALYTICAL EQUIPMENT		
Instrument/Make/Model	Analytical Principle	Last Multipoint Calibration
Horiba VIA 510-CO2-19GYCXEG	NDIR	Aug 09, 2018
Horiba MPA 510-O2-7TWMJ041	Paramagnetic	Aug 09, 2018

Triad Data Available Upon Request



\_\_\_\_\_  
Signature on file  
Approved for Release

# CERTIFICATE OF ANALYSIS

## Grade of Product: EPA Protocol

Part Number:	E03NI62E15A0224	Reference Number:	82-401044874-1
Cylinder Number:	SG9169108	Cylinder Volume:	157.2 CF
Laboratory:	124 - Riverton (SAP) - NJ	Cylinder Pressure:	2015 PSIG
PGVP Number:	B52017	Valve Outlet:	590
Gas Code:	CO2,O2,BALN	Certification Date:	Nov 18, 2017

**Expiration Date: Nov 18, 2025**

Certification performed in accordance with "EPA Traceability Protocol for Assay and Certification of Gaseous Calibration Standards (May 2012)" document EPA 600/R-12/531, using the assay procedures listed. Analytical Methodology does not require correction for analytical interference. This cylinder has a total analytical uncertainty as stated below with a confidence level of 95%. There are no significant impurities which affect the use of this calibration mixture. All concentrations are on a volume/volume basis unless otherwise noted.

Do Not Use This Cylinder below 100 psig, i.e. 0.7 megapascals.

ANALYTICAL RESULTS					
Component	Requested Concentration	Actual Concentration	Protocol Method	Total Relative Uncertainty	Assay Dates
CARBON DIOXIDE	17.00 %	16.58 %	G1	+/- 0.7% NIST Traceable	11/18/2017
OXYGEN	21.00 %	21.00 %	G1	+/- 0.5% NIST Traceable	11/18/2017
NITROGEN	Balance			-	

CALIBRATION STANDARDS					
Type	Lot ID	Cylinder No	Concentration	Uncertainty	Expiration Date
NTRM	12061336	CC360792	11.002 % CARBON DIOXIDE/NITROGEN	+/- 0.6%	Jan 11, 2018
NTRM	09061415	CC273526	22.53 % OXYGEN/NITROGEN	+/- 0.4%	Mar 08, 2019

ANALYTICAL EQUIPMENT		
Instrument/Make/Model	Analytical Principle	Last Multipoint Calibration
Horiba VIA 510-CO2-19GYCXEG	NDIR	Oct 30, 2017
Horiba MPA 510-O2-7TWMJ041	Paramagnetic	Oct 27, 2017

Triad Data Available Upon Request



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Signature on file  
Approved for Release

## INTERFERENCE CHECK

**Date:** 12/4/14-12/5/14

**Analyzer Type:** Servomex - O<sub>2</sub>

**Model No:** 4900


**Serial No:** 49000-652921

**Calibration Span:** 21.09 %

**Pollutant:** 21.09% O<sub>2</sub> - CC418692

INTERFERENT GAS	ANALYZER RESPONSE		% OF CALIBRATION SPAN <sup>(a)</sup>
	INTERFERENT GAS RESPONSE (%)	INTERFERENT GAS RESPONSE, WITH BACKGROUND POLLUTANT (%)	
CO <sub>2</sub> (30.17% CC199689)	0.00	-0.01	0.00
NO (445 ppm CC346681)	0.00	0.02	0.11
NO <sub>2</sub> (23.78 ppm CC500749)	NA	NA	NA
N <sub>2</sub> O (90.4 ppm CC352661)	0.00	0.05	0.24
CO (461.5 ppm XC006064B)	0.00	0.02	0.00
SO <sub>2</sub> (451.2 ppm CC409079)	0.00	0.05	0.23
CH <sub>4</sub> (453.1 ppm SG901795)	NA	NA	NA
H <sub>2</sub> (552 ppm ALM048043)	0.00	0.09	0.44
HCl (45.1 ppm CC17830)	0.00	0.03	0.14
NH <sub>3</sub> (9.69 ppm CC58181)	0.00	0.01	0.03
<b>TOTAL INTERFERENCE RESPONSE</b>			<b>1.20</b>
<b>METHOD SPECIFICATION</b>			<b>&lt; 2.5%</b>

<sup>(a)</sup> The larger of the absolute values obtained for the interferent tested with and without the pollutant present was used in summing the interferences.

  
 Chad Walker



## INTERFERENCE CHECK

**Date:** 12/4/14-12/5/14  
**Analyzer Type:** Servomex - CO<sub>2</sub>  
**Model No:** 4900  
**Serial No:** 49000-652921  
**Calibration Span:** 16.65%  
**Pollutant:** 16.65% CO<sub>2</sub> - CC418692

INTERFERENT GAS	ANALYZER RESPONSE		% OF CALIBRATION SPAN <sup>(a)</sup>
	INTERFERENT GAS RESPONSE (%)	INTERFERENT GAS RESPONSE, WITH BACKGROUND POLLUTANT (%)	
CO <sub>2</sub> (30.17% CC199689)	NA	NA	NA
NO (445 ppm CC346681)	0.00	0.02	0.10
NO <sub>2</sub> (23.78 ppm CC500749)	0.00	0.00	0.02
N <sub>2</sub> O (90.4 ppm CC352661)	0.00	0.01	0.04
CO (461.5 ppm XC006064B)	0.00	0.01	0.00
SO <sub>2</sub> (451.2 ppm CC409079)	0.00	0.11	0.64
CH <sub>4</sub> (453.1 ppm SG901795)	0.00	0.07	0.44
H <sub>2</sub> (552 ppm ALM048043)	0.00	0.04	0.22
HCl (45.1 ppm CC17830)	0.10	0.06	0.60
NH <sub>3</sub> (9.69 ppm CC58181)	0.00	0.02	0.14
<b>TOTAL INTERFERENCE RESPONSE</b>			<b>2.19</b>
<b>METHOD SPECIFICATION</b>			<b>&lt; 2.5%</b>

<sup>(a)</sup> The larger of the absolute values obtained for the interferent tested with and without the pollutant present was used in summing the interferences.

  
 Chad Walker

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**APPENDIX F**  
**LIST OF PROJECT PARTICIPANTS**

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The following Weston employees participated in this project.

Paul Meeter	Senior Project Manager
Jacob Little	Team Member
Kyle Schweitzer	Team Member
Austin Squires	Team Member
Chris Hartsy	Team Member